### **SESSION 8**

# GROUNDWATER EXPLORATION I



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#### 1 Introduction

**Ground water exploration** is the search for groundwater resources which can be exploited for the benefit of mankind.

Boreholes represent a large capital investment in a groundwater investigation; therefore, each borehole should be drilled to an optimum design and the location.

Optimum borehole design depends on a detailed knowledge of the geological functions and subsurface geometry in the area to be drilled.

This phased approach applies to both groundwater resource studies and to pollution investigations.

#### 1 Introduction

The principles of groundwater exploration are:

**Desk Studies** 

Remote Sensing

Well Inventories

Surface geophysics

**Exploration Drilling** 

**Groundwater Monitoring** 

### 2 Objectives of Groundwater Exploration

### 1. Development/exploitation of groundwater resources

Select areas where groundwater resources can be exploited (aerial photo interpretation studies, hydrogeological mapping, well inventories, ... etc)

Determine the quantity and quality of the resources that can be exploited without depleting the groundwater basin Locate springs and identify sites suitable for the installation of individual production wells and/or wellfields

Determine the depths of the wells to be drilled and the yield and the anticipated quality of the groundwater when production wells are installed.

### 2 Objectives of Groundwater Exploration

2. Protection of groundwater resources (control of hazards) (Contaminated Hydrogeology)



#### 3.1 Topography and Geology

Topographical maps (Figure 3.1) showing topography, wadis, vegetation, roads and communities can give a good picture about the investigated area;

Scale of maps 1:100,000 – 1:250,000 regional review

1:25,000 - 1:50,000 detailed review

Springs and areas with shallow groundwater levels may be shown on the map indicating the presence of groundwater resources;

Topographical area like rivers, wadi intersection and coastal areas may indicate the presence of groundwater;

The slope of the terrain shown on the map usually indicates the direction of shallow groundwater flow.

Geological borehole logs are mainly compiled on the basis of rock samples (geotechnical assessments, oil and gas exploration, ... etc) (see Figure 3.2)

The logs normally consist of written descriptions of the geology (lithological description of rock types) (see Figure 3.2)

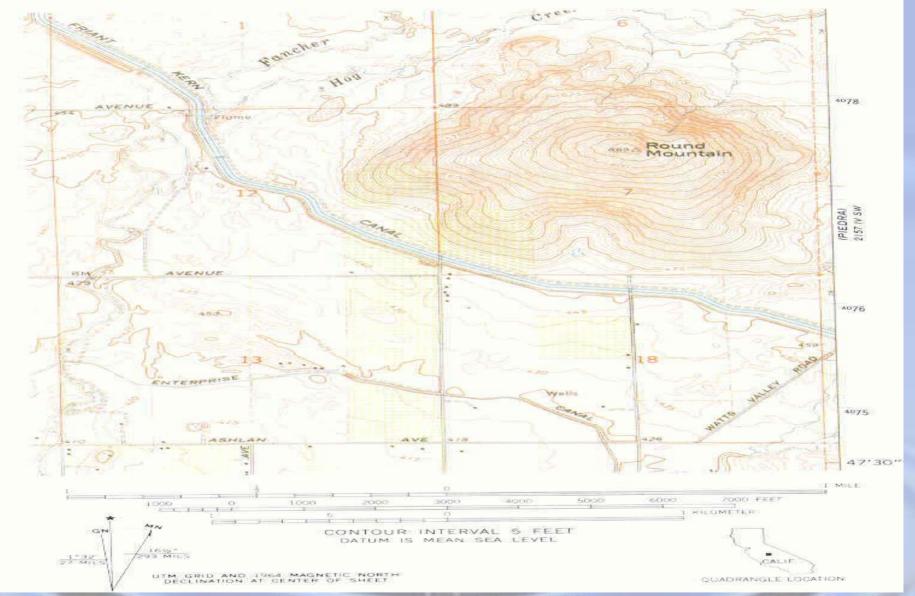
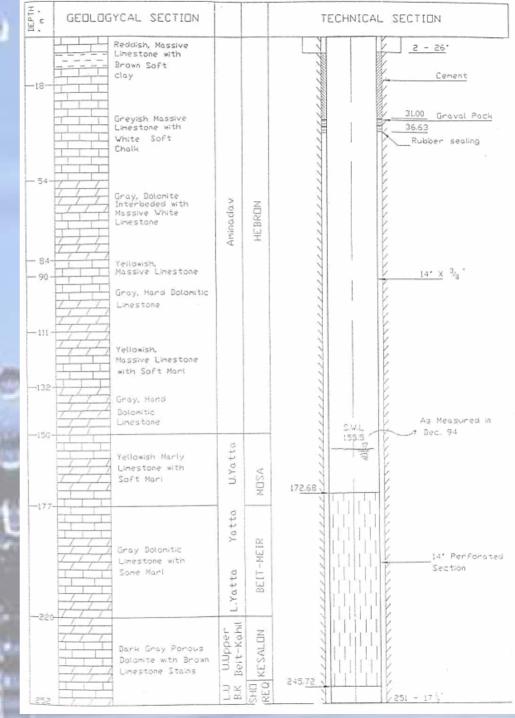


Figure 3.1: Topographic maps are useful to drilling contractors because they indicate the nature of the terrain, the presence of streams, and lakes, and the location of highways, buildings and railroads.

Figure 3.2 Vertical
Geological section and
technical section for Ein
Samia Well (ESW2a)



Topographical area like rivers, wadi intersection and coastal areas may indicate the presence of groundwater;

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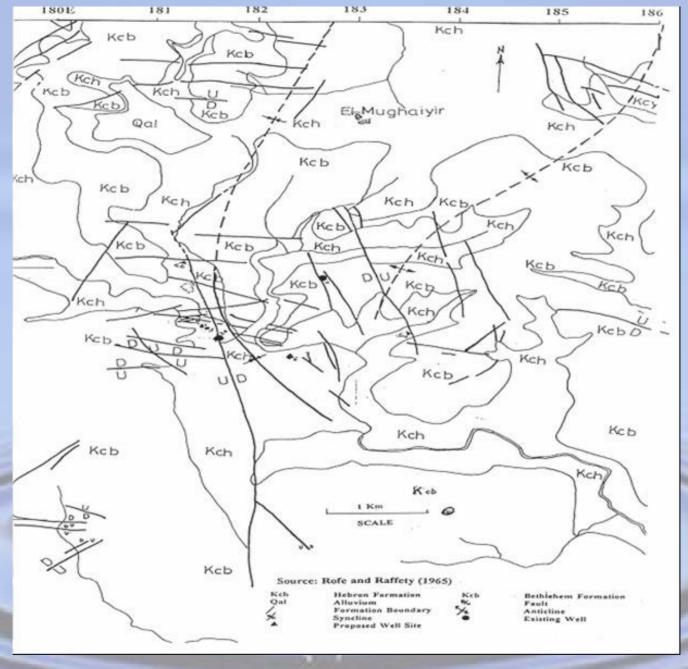


Figure 3.3 Geological Map of the Ein Samia Area

#### 3.2 Hydrometeorological Methods

When precipitation over evaporation is large then the recharge into the groundwater basin is large (that is when the geological formations area sufficiently permeable)



#### > Springs indicate the presence of groundwater resources

- Springs issue as a result of contact between limestone and chalk (or shale or marl) indicate that one rock type acts as the permeable groundwater supplying formations and the other as the impermeable rock forcing the water to land surface.
- Springs at fault zones: if the fault zone acts as an impermeable barrier, water levels upstream will rise (shallow water levels) and springs may issue upstream. This indicates that the water levels downstream are likely to be deep and thus reducing the possibility of groundwater exploitation.
- ✓ Springs flow is in fact groundwater discharge from related permeable formations.

  Depending on the amount of groundwater recharge one can generally state that the larger the spring the larger is the groundwater basin which contributes to spring flow.
- ✓ By considering a geological map together with spring flow records, the potential of the local aquifer in the investigated area can be identified.

#### Wadis and Discharges

- ✓ If the pattern of a wadi runoff is dense, then the permeability of the (underneath) formations is low. Most of the precipitation will become surface runoff thereby creating this dense pattern.
- ✓ When the pattern is not very dense then the permeability of the formation is high: much of the precipitation will infiltrate and there will be hardly any surface runoff to create a dense pattern. Thus, these wadis are major sources of groundwater pollution should the wadis become contaminated

#### 3.3 Available Groundwater Data

- ➤ Geophysical reports: identify sections with interpreted resistivities;
- **Well site reports**: you may find geological logs, geophysical logs, water sample analysis, well design, pumping test data, groundwater level records, pumping rate data ... etc;
- Maps and sections;
- Formula Groundwater assessment reports;

#### **3.4 Satellite Imagery Studies**

Figure 3.4). The full light spectrum may be used when taking these pictures or certain wave lengths of the spectrum may be selected. Groundwater related features on satellite pictures can be detected by bare eye and by using a stereoscope.

The best known picture are the **LANDSAT** images taken by satellites launched by the USA and the **SPOT** images produced by satellites brought into orbit by France.

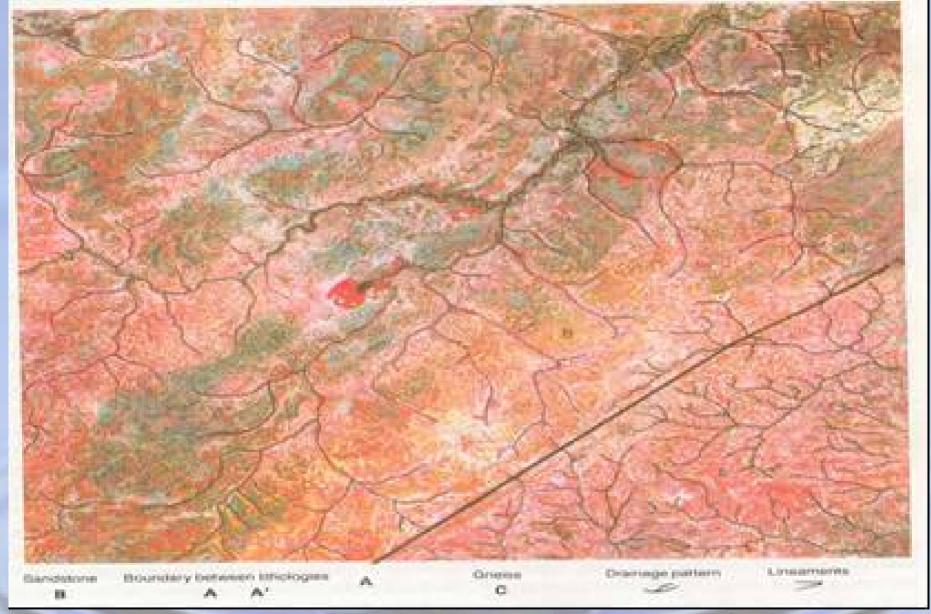


Figure 3.4 Computer-enhanced LANDSAT color composite of Bobo-Dioulasso Area, upper volta, West Africa. Acquired on March 31, 1976.

#### **3.4 Satellite Imagery Studies**

#### > Interpretations

- ✓ Satellite images are very handy tools to obtain a regional overview of the geology.
- ✓ The images can be used to get an impression on the regional drainage system.
- ✓ Combining the geological and surface water information, a hydrogeological assessment of the "imaged area" can be made.
- ✓ The images can be used to identify lineaments extending over several tens or even hundreds of kilometers.

### 3.5 Aerial Photography Analysis and Fracture Traces Technique for Sitting a Well

#### **General Notes**

Aerial photos are taken from an aeroplane. The plane follows a flight path covering completely the selected area. The photos taken are partly overlapping each other in order to be able to obtain 3-dimensional view with a stereoscope. The instrument consists of two sets of mirrors and lenses which produce the three dimensional view (see Figure 3.5).



**Figure 3.5** Groundwater related features on satellite picture can be detected by bare eye and by using a **Stereoscope**.

### 3.5 Aerial Photography Analysis and Fracture Traces Technique for Sitting a Well

- Stratgraphical layering of consolidated sedimentary rocks can be observed as 'bands' on the photos.
- Shales, mudstones and siltstones can be recognized by 'bands' of darkgrey to black tones.
- Not very permeable carbonate rocks such as limestone and dolomites can be identified by their massive banding and usually lighter tones.
- Permeable limestones and dolomites are often identified by the presence of karstic features including **sinkholes** (see **Figure 3.6**).

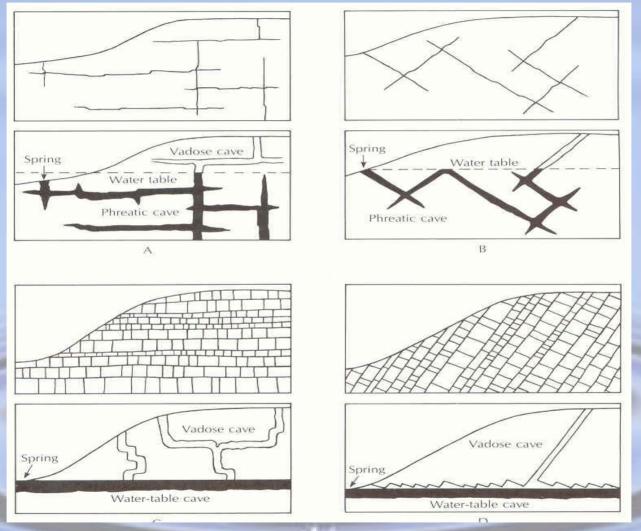


Figure 3.6 Effects of fissure density and orientation on the development of caverns

- River alluvial deposits (gravel, sands, clays and silt) can be recognized from the presence of river terraces.
- From above, the identified on the aerial photos can be classified as aquifers, aquitards, ... etc.
- The type, location, and size of the aquifers present in the area give an indication of the groundwater potential.
- In the **saddles and crests of large folds**, fissures have often formed as a result of lateral issues.
- The presence of a spring is indicated by dense vegetation.
- For Groundwater is known to be concentrated in fracture zone found in many different rock types (see **Figure 3.7**).

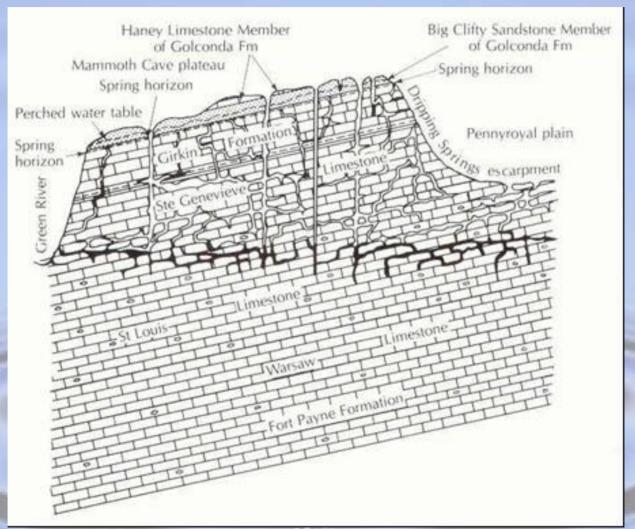


Figure 3.7 Groundwater flow in the carbonate aquifer is from south to north

- In the identification of fracture traces on aerial photographs, a low magnification stereoscope is generally used. (60% stereoscopic overlapping, 1:20,000 scale. 20% overlapping between flight lines).
- Possible fracture traces are indicated by drawing on the photograph. One problem in identification is the confusion of linear features of human origin (fences, roads, ... etc.) with natural linear feature. Following the mapping of linear features on air photos, it is necessary to make a field check.

- In crystalline rock areas, high-yield wells are generally associated with fracture traces which may not be necessarily correspond to topographic lows.
- A **zig-zag** offsets in the regional valley alignment assure well developed fracture traces.
- Openings in the fault zones and at the weathered parts of joint systems may indicate exploitable groundwater resources.

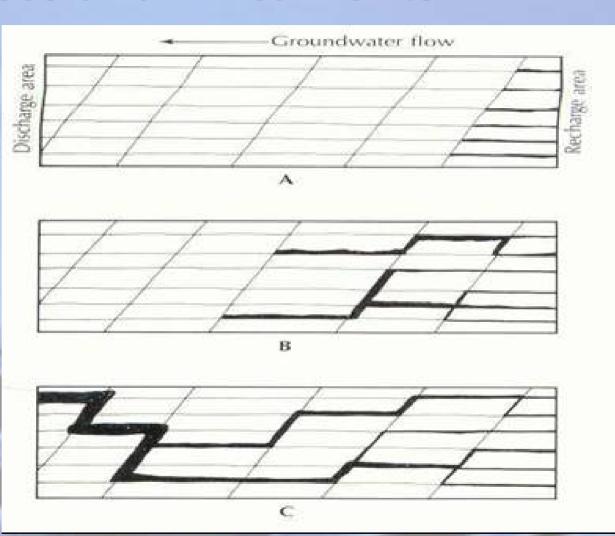
- Fracture traces are located by study of linear features on aerial or satellite photographs.
- Natural linear features from **300 m** to around **1500 m** in length are fracture traces.
- Natural linear features **greater than 1500 m** in length are termed **lineaments**. Some lineaments are up to 150 km long.
- Fracture traces are surface expressions of joints, zone of joint concentration or faults.

➤ On air photos, natural linear features consist tonal variation in soils:

- ✓ Alignment of vegetation patterns;
- ✓ Straight stream segments or valleys;
- ✓ Aligned surface depressions;
- ✓ Gaps in ridges;

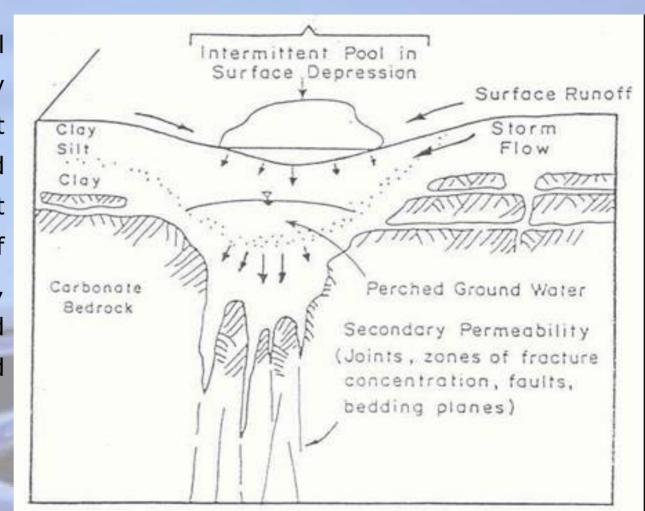
It is generally believed that the joint sets tend to be perpendicular. They are known to extend to a depth of 1000 m at one Arizona location as an example (see Figure 3.8).

Figure 3.8 Growth of a carbonate aquifer drainage in the system starting recharge area and growing toward the discharge area. A. At first, most joints in the undergo recharge area solution enlargement. B. As the solution passages grow, they join and become fewer. C. Eventually, one outlet appears at the discharge zone.



- Fracture zones are less resistant to erosion. Hence, valley and stream segments tend to run along fracture zone.
- Fracture traces and lineaments appear to have their greatest utility in rocks where secondary permeability and porosity dominate and where intergranular characteristics combine with secondary openings influencing weathering and soil water and groundwater movement. Fracture traces and lineaments are considered surface manifestations of vertical to near-vertical zone of fracture concentration.
- Fracture traces may be related to regional tectonic activity. They tend to be oriented at a constant angle to the regional structural trend. However, the orientation appears to be independent of local folds.
- Fracture traces in carbonate rocks are typically areas of solution. Aligned sinkhole or surface sags are typical surface expressions (see Figure 3.94,14

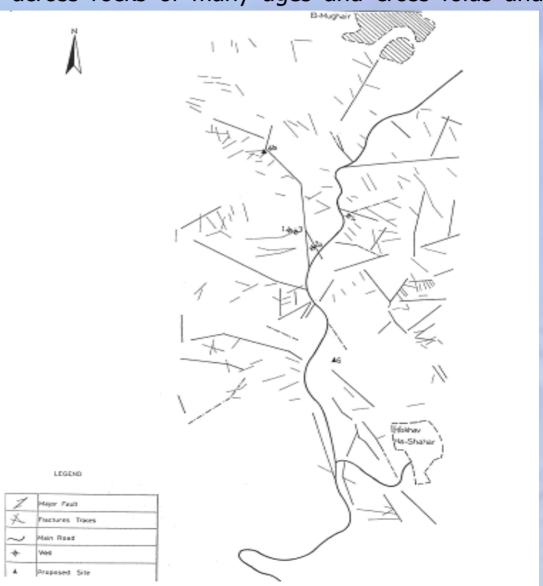
**Figure** Differential 3.9 weathering along secondary openings in bedrock result in the surface sag and depressions that concentrate surface runoff perched ponds, groundwater lenses and increased infiltration and solution of bedrock.



Lineaments are known to cut across rocks of many ages and cross folds and

faults (see Figure 3.10).

**Figure 3.10** Lineaments and fractures map of Ein Samia

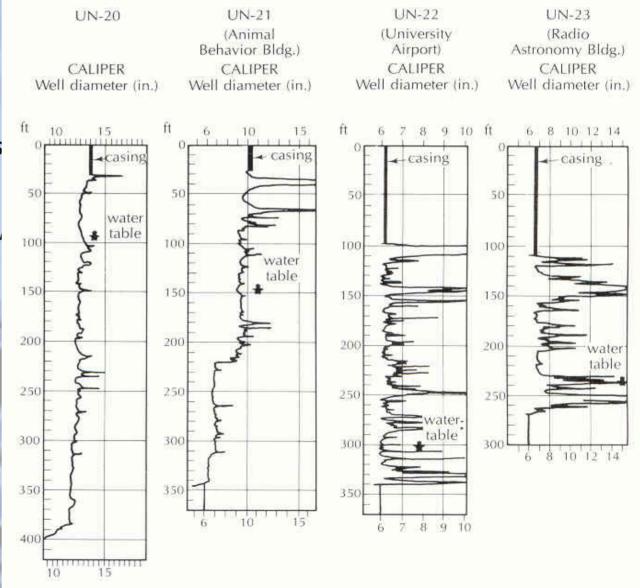


- Lineaments have been observed to be parallel to the major joint sets in flat-lying or gently dipping strata, but this is not the case if the strata are steeply dipping.
- If surface area separated by major faults, the individual fault blocks may have fracture traces of different orientation.
- The majority of fracture traces control is evident have been described as having a "stair-step" pattern.

- Statistical studies of wells in carbonate terrane have shown that those located on fracture traces, either intentionally or accidentally have a greater yield than those not on fracture traces.
- Fracture traces are known to reveal narrow zones (2 to 20 m wide) suitable for groundwater prospecting, high permeability and porosity avenues 10 to 1000 times that of adjacent strata.
- Caliper logs of wells on fracture traces in carbonate-rock terrane showed many more cavernous opening and enlarged bedding planes than logs of those wells drilled in interfracture areas (see Figure 3.11).

#### **Figure 3.11**

Caliper logs of wells in an area of carbonate rocks in central Pennsylvania. Wells UN-20 and UN-21 were drilled in interfracture area, Wells UN-22 and UN-23 were located on fracture traces



> Fracture traces technique is used to locate high-yield wells (see Figure

3.12).

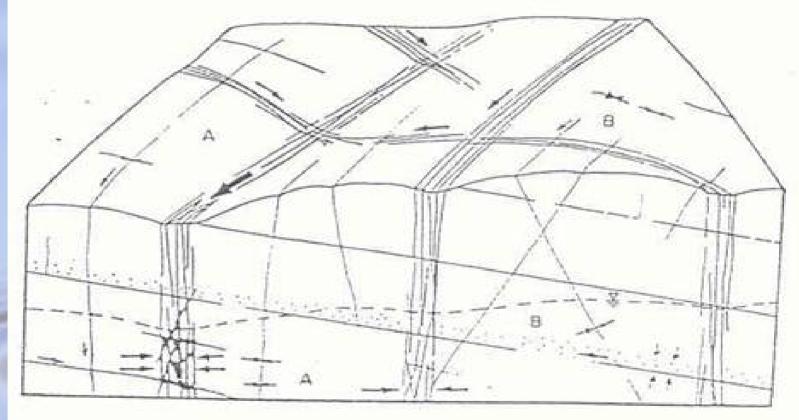


Figure 3.12 Massive bocks of carbonate rock interlaced with high avenues of permeability development along zones of fracture concentration. Transmission and storage properties afforded by intergranular and vugular openings within selected beds, bedding plane partings, joints and fault zones.

### **Fracture Traces and Lineaments**

### > The problems with lineaments and fracture traces:

- ✓ What are the depth and width of lineaments and fracture traces!!;
- ✓ Accurate location on the ground!;
- Well yield depends also on well radius, well depth and diameter, casing length, method of drilling, degree of well development, depth to water table, presence of various changes of rock type, dip of beds, topographical settings, rock type, type of fold structure, presence and type of joints, number and type of zones of fracture concentration, ... etc.;
- If fracture traces are absent from a property on which water is required, the use of expert advice would not help except to point out the increased risk of obtaining a low yield.

- ➤ Well sitting is important prior to any water resources development project.
- Site studies are necessary prior to construction of projects as sanitary landfills, land-treatment systems for wastewater, surface mines, power plants, artificial-recharge lagoons, nuclear-waste repositories, dams and reservoirs.
- The greatest yields come from wells located at the **intersection** of two fracture traces or more (see **Figure 3.13**).

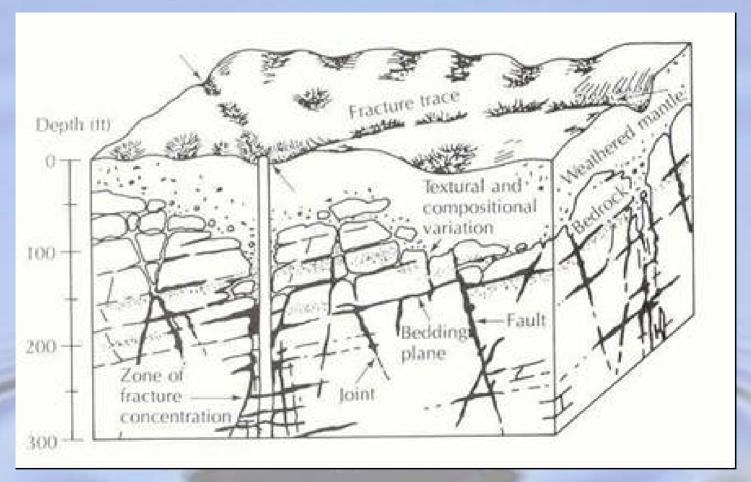


Figure 3.13 Concentration of ground water along zones of fracture concentrations in carbonate rock. Wells that don't intercept an enlargement fracture or a bedding plane may be dry, thus indicating a discontinuous water table.

- Some investigations failed to correlate high well yields and well locations with respect to fracture traces sites in carbonate rocks because:
  - ✓ Fracture traces were not mapped correctly;
  - ✓ The width of influence of fracture trace was not known;
  - ✓ Wells did not hit the center lines of fracture traces;

- Some variability in yield remains for wells located on lineaments due to the fact that joints, fractures, bedding plane partings and secondary weathering is not equally well developed beneath lineaments and an element of chance and variability of penetrating openings will always remain when drilling on fracture concentration. Variable fracture development has been observed in cross-sectional views.
- The same variability of fracture and joint development beneath lineaments has not been documented but it is recommend that all lineament well sites also located on fracture trace intersections or on single fracture traces to increase the probability of penetrating the maximum number of secondary openings.

- Fracture-trace analysis is also very useful in determining the locations of groundwater monitoring wells. Because groundwater flow preferentially follows the most permeable pathway, monitoring wells should be located on fracture traces.
- It should be noted that wells located in valley bottom settings show higher yields than wells located on adjacent uplands (see **Figure 3.14**).

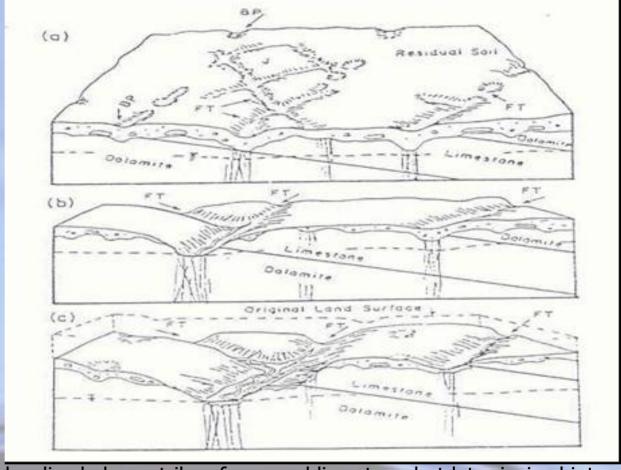
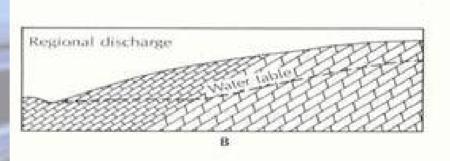


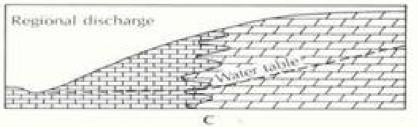
Figure 3.14 Valley development localized along strike of exposed limestone but later incised into underlying gently dipping dolomite. In (a) differential weathering along bedding planes (BP), joints (J), and zones of fracture concentration (FT) produce surface sags and depressions that concentrate surface runoff, facilitates infiltration and erosion of residual soils. In (b) weathering and erosion are enhanced along soluable limestone and a master drainage system is fixed in its position. Increased runoff facilitates erosion until groundwater drains are established. In (c) the land surface is lowered and the valley is incised into less soluable dolomite bedrock.

The **poorest sites** were expected within interfracture trace areas, on **upland**, on **synclinal troughts**, where bedrocks dips were **in excess of 30°**, the water table is deep and shale was exposed (see **Figure 3.15**).

#### **Figure 3.15**

Geologic conditions resulting in a difference in hydraulic conductivity and, hence, a difference in the water-table gradient.







### **► Where Shall We Drill a Well?**

- ✓ Water will not flow uphill;
- ✓ Water will not flow through clay or dense rock!!!;
- ✓ Water flows freely through the fissures and between stones;
- ✓ On a single fracture trace or intersection of two or more fracture traces;
- ✓ Wells drilled in anticlines are better producers than wells drilled in synclines;
- ✓ Wells in beds dipping at less than 15° had higher yields than wells in steeper beds;

What other considerations should be taken in sitting a well.

Your choice of well site will affect the safety and performance of your well. As you examine various sites, remember to consider any future development plans for your farm or acreage such as barns, storage sheds and bulk fuel tanks. You must also consider provincial regulations that dictate well location.

Most contaminants enter the well either through the top or around the outside of the casing. Sewage or other contaminants may percolate down through the upper layers of the ground surface to the aquifer. The following criteria are intended to prevent possible contamination of your well and the aquifer. It is both your and the driller's responsibility to ensure that:

- ✓ The well is accessible for cleaning, testing, monitoring, maintenance and repair;
- ✓ The ground surrounding the well is sloped away from the well to prevent any surface run off from collecting or ponding;
- ✓ The well is up-slope and as far as possible from potential contamination sources such as septic systems, barnyards or surface water bodies;
- ✓ The well is not housed in any building other than a bona fide pumphouse. The pumphouse must be properly vented to the outside to prevent any buildup of dangerous naturally occurring gases
- ✓ The well is not located in a well pit.

### Minimum distance requirements.

Provincial regulations outline minimum distance requirements as follows. Equivalent imperial distances in feet are rounded up to nearest foot. The well must be:

- √ 10 m (33 ft.) from a watertight septic tank;
- √ 15 m (50 ft.) from a sub-surface weeping tile effluent disposal field or evaporation mound;
- √ 50 m (165 ft.) from sewage effluent discharge to the ground;
- √ 100 m (329 ft.) from a sewage lagoon;
- √ 50 m (165 ft.) from above-ground fuel storage tanks;
- √ 3.25 m (11 ft.) from existing buildings;

### Minimum distance requirements.

- ✓ 2 m (7 ft.) from overhead power lines if: the line conductors are insulated or weatherproofed and the line is operated at 750 volts or less;
- ✓ 6 m (20 ft.) from overhead power lines if the well: does not have a pipe and sucker rod pumping system has a PVC or non-conducting pipe pumping system has well casing sections no greater than 7 m (23 ft.) in length;
- ✓ 12 m (40 ft.) from overhead power lines for all other well constructions;
- ✓ 500 m (1,641 ft.) from a sanitary landfill, modified sanitary landfill or dry waste site.

### 3.6 Hydrogeological Mapping and Well inventories

Hydrogeological mapping is the study of rock types and drainage conditions in the field with emphasis on hydrogeological aspects (see **Figure 3.16**);

#### **Stratigraphic section of the West Bank**

Period		Age		Graphic Log	Typical Lithology	Formation (Palestine terminology)	Sub- Formation	Group	Formation and Group (Ismeli Terminology)	Hydro- stratigraphy	Typical Thickness (m)
-		Hotocene		1.00.	Nan (surface crust) and alluvium gravels and fan deposits	Alluvium			Alluyipm	Local Aquifer	0 - 100
Quaternary		Prejatoppenie			Thinly laminated man with gypsum bands and poorly soniad graves and patitives	Lisen		Dens See	Kurkar Group (W.A. Basen) Servin and Lean formolieris		10 - 200
	Neogone	Pincene Mixtene			Conglomerates, mart, challs clay and limestore	Beida		Noegene Conglom- erates	Saqiye Groop	Sattype (Aquitant) (Aquitant) (Especial Beida (Local Aquifor) Palestica	20 - 200
19cttory				HITHLINE	Reefal Imestone	Jeon	Jenin 4	Jenn	'Aveidat Group  Mt. Scopus Group	Aquiter	90 - 670
190	8:	Eccene		HIERATION	Nummulitic bedded limestone		Jenn 3				
	Paleogoop	(Lower -		11241124	Nummulitic limestone, chalk		Janut 2			William	
	T.	Middle)			Chalk, nummulisc limestone		Jenin 1			Aquitard	
		Paleoceni	è	1111	MarL chalk						40 - 150
		Maintri Dani	chium	+ + +	Charle mart	Al-Ahmar		Nation		(Local Aquifer)	90.1100.1
		2 Carnot		all the sale	Mein chert, phosphate	Wadi Al-Qill				Aquiclade	10 - 120
		A Conser Santo	ciar- nian	1-1-1	Chalk and ched	Abu Dis				Soloimios :	0 - 450
	The -	Turonu		21,121	White timestone strollines dolonite and thin bedded timestone	Jeruselem			Bina		40 - 190
5008	Botto				Dolomite soft	Bestighen	Upper		Weradim		
		16	10		Chalky imestone chalk		Lower		Kefar Sha'ul	Aquiller Aquiller	50 - 210
		Cenominim	Cerominian		Karálic dolornile	Hebron		W. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	Amminadav	sfer System	65 - 160
Cheteceous			16810	MITTES.	Yellow mart	Yatta	Upper [Middle	Ramaliah (West	Moga	"Amillard"	50 - 125
a			07		Limestone & dolostone, chark, (clay)	T. T	FOMBS.	Bank)	Sed Mer	94	
					Reefal limestone	Upper	UBK2		Kesalon	Me de la companya de	10 - 20
		Albien			Dolomite imestone, interbedded with man	tielt Kahil	UBK1		Soraq	10000	60 - 130
					Dolomite		LBK2		Givat Ye'ann	Aquifer	40 - 90
	GE.				Karstic Imestone	Bell-Kehit	LBK1		Kefira		100 - 160
	100			2000	Mari, marty nodular limestone	Qatana			Catana	Aquitard	42
					Marty limestone and limestone	Ein Qinya		Kobar	Ein Qinya	Aquited (Local Aquifer)	55
				~~~~	Shale	Tammun			Terronce	Aquiciude (Local Aquifer)	300+
		Appa	Appan ST IOT I		Shale and limestone	Em Al-Assad		-	CNIMICONNE.	(Loom Aguiler)	20+
				121 TOT	Marly limestone, sandy	Nabi Sand		Kumub	Hatira	Aquifer	20+
		Neocor	ciari	100000000	Sandstone Volcanics	Ramali Tayase		CARCINES.	100000	1.12400.00	35
	1380	Dxfordian			Mari interbeddett with chalky.limestone	Malen	Upper Maleh	:	Arad Group	Aquitand	100 - 200
Aurasan				1414141417	Dotomicc limestone, jointed and lurralic		Lower Maleh	+	Sales a second	Aquifer	50 - 100
	ENI	Delomite			Mart.	* Megafauna			Chalk	Ē	Sandst

#### **Northern West Bank cross section**

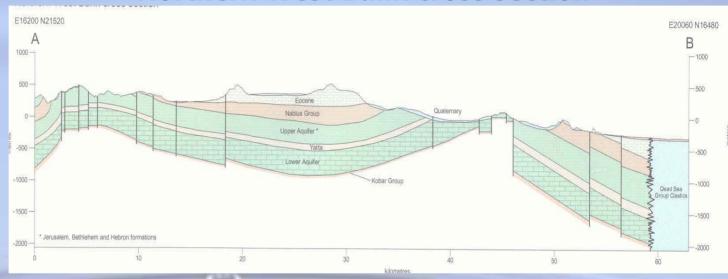
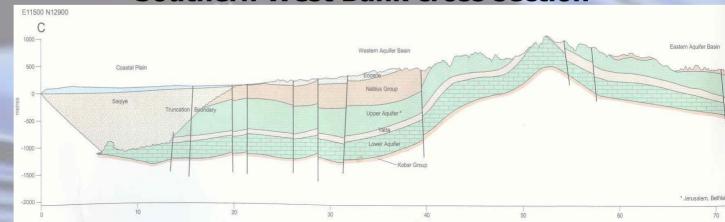


Figure 3.16
Hydrogeological
Map of the West
Bank

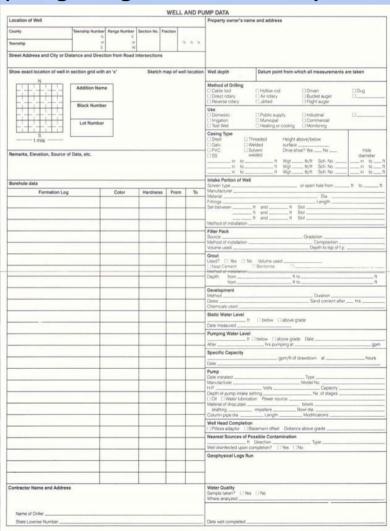
#### **Southern West Bank cross section**



Well inventories is the preparation of inventories of well existing in an area while aiming to analyze the local hydrogeological conditions (see

Table 3.1);

Table 3.1 Well and Pump Data



- Mapping and inventory activities may lead to full hydrogeological analyses by itself and to determine planning of any exploration program;
- At sites the following features are of interest:
  - ✓ Mineral content of rock type;
  - ✓ Colours;
  - ✓ Layering of rocks and bed thicknesses;
  - ✓ Dip of beds;
  - Presence, types and dimensions of faults and joints;
  - ✓ Fossil content;
  - ✓ Evaluated rock types;
  - ✓ Porosity of the rocks;
  - ✓ Degree of cementation;
  - ✓ Degree of weathering.

- Well inventories cover all type of wells, production, monitoring, abandoned, exploration, ... etc.
- Table 3.2 shows the index for Model Map

Table 3.2 Index for the Model Map

#### **Table 3.2** Index for the Model Map

	A A			
C. GEOLOGY GEO	DLOGIE GEOLOGIA ГЕОЛОГИЯ	E.6	£	Disappearance point of stream
la .	Contact between different units, lines broken where approximate	1		Point de disparition d'un cours d'eau Punta de desparición de un curso de agua
/	Contact entre des unités différentes, en traits			Пункт исчезновения водотока
	interrompus si hypothétique Contacto entre unidades distintas, en trazos	9		Marsh
	discontinuos si es hinotética	业	AL.	Marais
	Контакт между различными единицами, если гипотетический пунктиром	1 '	ML	Marisma Болото
2 /		-		
100	Depth of top of the limestone Profondeur du toit de la calcaire	10	~	Area inundated during floods Terrain inondé pendant les crues
/*	Profundidad del techo de la caliza	-	,-L	Terreno inundado en las crecidas
	Абсолютная отметка кровли известняка			Участок, затопленный паводковыми водами
/	Depth of top of the sandstone	111	2.5	Surface-water divide
100	Profondeur du tout du grès Profundidad del techo de la arenisca	1		Ligne de partage des eaux superficielles Linea divisoria de las aguas superficiales
1	Абсолютная отметка кровли песчаника			Водораздел поверхностных вод
1. /				
5	Strike and dip Direction et pendage	12		Spring Source
	Dirección y buzamiento	1	0"	Fuente
	Простирание и падение			Источник
. 1	personal control of the control of t	13		Group of springs
0	Axis of anticline, with direction of axial plunge Axe anticlinal, avec direction de plongement axial		5	Groupe de sources Grupo de fuentes
	Eje anticlinal, indicando su dirección de buzamiento			Группа источников
	Ось антиклинали и направление ее погружения	14		Thermal or thermominural spring (see G.4. and G.6.)
/		- 6	3	Source thermale ou thermominerale (voir G.4. et G.6.)
7	Axis of syncline, with direction of axial plunge	1	9	Fuente termal o termomineral (ver G.4. у G.6.) Термальный или термоминеральный источник
*	Axe synclinal, avec direction de plongement axial Eje sinclinal, indicando su dirección de buzamiento			(cm.G 4 n G6)
/ / /	<ul> <li>Еје sinclinal, indicando su dirección de buzamiento</li> <li>Осъ синклинали и направление ее погружения</li> </ul>	15		Natural pond or waterhole with no outlet
		-	7	Etang ou point d'eau naturel sans écoulement Laguna o punto de agua natural sin escorrentia
10	Fault, with direction of downthrow side, line broken	1	9.	Бессточний естественный водоем или
/	where uncertain			водохранилище (пруд)
/	Faille, avec direction du sôté affaissé, en traits interrompus si hypothétique	16		Lake
	Falla con dirección del labio hundido, en trazos discontinuos, si es supuesta		100	Lago
/	Сброс с указанием опущенного крыла пунктиром сброса, если гипотетический			Osepo
13	пунктиром сороса, если гипотетический			HYDROLOGY HYDROLOGIE DES
D. LITHOLOGY LIT	THOLOGIE LITOLOGIA ЛИТОЛОГИЯ			INS HYDROLOGIA DE LAS
3			SUBTERR	
3	Sands and gravels Sables et graviers	ДИНАМ	ика подз	ЕМНЫХ ВОД
0.0.0.0	Arenas y gravas	1	/	Groundwater contours (piezometric surface on the section) for the limestone
	Пески, галечники и гравий.	1		Courbes isopièzes (niveau piézométrique de la
6	Sandstones with conglomerates	1 2	100	coupe) pour la calcaire Curvas isopiezas (nivel piezométrico en la sección)
	Grès avec conglomérats	/		por la caliza
* * * * * * * *	Areniscas con comglomerados Песчаники с конгломератами			Изогипсы — (пьезометрическая поверхность разреза) для известняка
				Groundwater contours (piczometric surface on the
7	Limestones		1	section) for the sandstone
1	Calcaires Calizas		5	Courbes isopièzes (nivcau piézométrique de la coupe) pour le grés
	Известняки	1		Curvas isopiezas (nível piezométrico en la socción)
13	W	1		рог la arenisca Изогипсы (пьезометрическая поверхность
13	Extrusive rocks, fissured Roches extrusives, fracturées			разреза) для песчанника
-1-1-1-1-	Rocas efusivas, fisuradas	2		Direction of groundwater flow with velocity in m
	Экструзивные породы, трещиноватые			per day Sens d'écoulement de la nappe, avec la vitesse en m
E. HYDROGRAPHY	HYDROCRAPHIE			par jour
HIDROGRAFIA			10	Dirección de la escorrentia de la capa acuifera, con la velocidad en m por día
1	Perennial stream with direction of flow			Направление движений подземных вод с скоростью в м/сут
	Cours d'eau pérenne, avec sens d'écoulement			
1	Curso de agua perenne con dirección de la circulación	3		Groundwater divide Ligne de partage des caux souterraines
	Постоянный водоток с направлением течения		0	Linea divisoria de las aguas subterráneas
,	течения	0		Граница бассейна подземных вод
4	Seasonal stream with direction of flow	5	THE PERSON NAMED IN	Boundary of area of artesian flow, with date
*	Cours d'eau saisonnier avec sens d'écoulement	1960	Hanne	Limite d'extension de la zone d'artésianisme, avec date
1	Curso de agua estacional con dirección de la circulación	THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN TW		Linea de la superficie de la zona artesiana, con la fecha
/	Сезонный водоток с цаправлением течениия	erimin.		Граница артегнанского бассейна с датой
			_	

F.11	Lines of equal thickness of saturated zone for the limestone Courbes degale puissance de la couche saturée pour la ciclaire la ciguit potencia de la capa saturada por la ciclaire su figuit potencia de la capa saturada por la caltie puissance su	FORAGES, PUITS SONDEOS, POZOS	LLS AND OTHER WORKS ET AUTRES OUVRAGES SY OTRAS OBRAS ROALLA M ДРУГИЕ ВЫРАБОТКИ Day well, non-netrain and proper laber Poto excayado, en una capa aculfera libre Kozanada roanoscua e Genanospono aconoscua ropanoure Genanospono aconoscua ropanoure
G. HYDROCHEMISTI HIDROQUIMICA	Естественное питание водоносного горизонта в мм/год  RY HYDROCHIMIE	. t	Dug well, artesian, not overflowing Puits crousé, dans une nappe captive, mais non-jaillissant Pozo excavado, artesiano no surgente Konzinsil kononcie is namopianzi nonosocienas горизонта, мо не самоналивалющийся
2 And Andrews	Depth of interface between fresh and saline groundwater Profondeur de la surface de séparation entre l'eau	్	Dug well, artesian, overflowing Puits creusé artésien (jaillissant) Pozo excavado, artesiano (surgente) Коланый кололец аргезнанский (самонэливающийся)
1000	douce et l'eau salée Profundidad de la superficie de separación entre et agua dutce y la sulada Глубина замегания поверхиюсти раздела просных и солсных вод.	Ŷ	Recharge well Pults creusé, d'injection Pozo excardo de recarga Поглошающий колодец
5 100	Water temperature in degrees Celsius Température de l'eau en degrés Celsius Temperatura del agua en grados Celsius Температура воды по Цельсию.	•	Dry well Puits cressé, sec Pozo excavado, seco Cyxoñ kononeu Drilled well (see also H.3.)
4 and 6	Dug well with sodium chloride water, not fit for use Puits creusé avec eaux chlorurées sodiques, non utilisables Poro excavado con aguas clorurados sódicias, no utilisrables	8	Puits foré (voir aussi H.3.) Pozo perforado (ver también H.3.) Byponoli kononeu (em. ranke H.3) Spring used for supply Captage de source Captación en una fuente
0	Копаный колоден с клоридной натриевой водою, менспользуемой.  Dug well with sodium chloride water, 2 · 4 g/l Pults creusé avec eaux chlorurées sodiques, 2 · 4 g/l Pozo excavado con aguas choruradas sodicas, 2 · 4 g/l	9	Kantriponainiadi lictovenus Drainage gallery Galerie drainante Galeria de drenaje Дренажная галлерся
	Konanый колодец с хлоридной натриевой водного 2—4 г/л  Dug well with sodium chloride water, 4 - 8 g/l Puits creusé avec caux chlorurées sodiques, 4 - 8 g/l	10	Groundwater pumping station Captage of eau souterraine Estación de bombeo, de agua subterranea Насосная станция из подземых вод
0	Pozo excavado con aguas cionuradas sódicas, 4 - 8 g/l Konansilis konzocate c xnopiciusofi nazpiecaoli nozioso 4 → 8 f/a Dug well with sodium chloride water > 8 g/l Puits creusé avec auss chlorurées sodiques, > 8 g/l Pozo excavado con aguas ciorradas sódicas, > 8 g/l	11 <b>⊚</b> °	Groundwater observation station, with recorder Station de jaugeage de l'eau souterraine, avec enregistreur Estación de aforo de aguas subterráneas, con régistrador Наблюдательная станция за режимом
	Four extra out con agust cioruratas souras, > 8 gr Komanuali komonette x mopiquisoli marpiesoli mognio > 8 r/m.  Group of springs with magnesium sulphate water, > 8 grl	۵	подземных вод  Decade station Station de la Décennie hydrologique Estación del Decenio hidrológico Станция гидрологического досятилетия
•	Гозире de sources avec eaux sulfatées magnésiennes, > 8 gfl Grupo de luentes con aguas sulfatadas magnesianas, > 8 gfl Группан источняков с сульфатной магиневой водою > 8 г/л.	12	Stream gauging station, with yearly average flow and area of catchment Station de jusquege d'un cours d'eau, avec débit moyen annuel et surface du bassin de drainage Estación de aforo de un curso de agua indicando el caudal media onual y la superfeió de la cuenca de caudal media onual y la superfeió de la cuenca de
0	Group of springs with sodium chloride water, 4.8 g/l Groupe de sources avec eaux chlorurées sodiques, 4.8 g/l Grupo de fuentes con aguas choruradas sódicas, 4.8 g/l	17	dereaje Наблюдательная станция на водотоке, умальнается среднегодовой расход и площать дренируемого бассейна Dam (with capacity of reservoir in million m³) Barrage de retenue ou de defiyation (avec capacité
8	Группа источников с хлоряданой натрякевой волюно 4—8 г/л  Highly polluted stream (organic pollution)  Cours d'eau fortement pollué (pollution organique)	O,	de reservoir en millions de m <sup>*</sup> ) Presa de embalse o derivación (con capacidad en milliones de m <sup>3</sup> ) Плотина водохранилница с емкостью в млн. м <sup>3</sup>
	Curso de agua muy polucionada (polución organica) Сильно загрязненный водоток (органическое загрязнение).	19	Canal, irrigation canal (perennial waters) Canal, canal d'irrigation (cau pérenne) Canal, canal de irrigación (agua perenne) Канал, ирригационный канал (постоянный водоток)
	Stream with high salinity Course deau sale Curso de agua salada Conessañ водоток	20	Canal, flood waters Canal, eaux de crue Canal, taguas de crecida) Kasian, (rasouxomae nonia)
10	Salt lake Lac salé Lago salado Conence osepo	21	Drainage canal Canal de drainage Canal de drenaje Apetaswanki santan

### **SESSION 9**

# GROUNDWATER EXPLORATION II



### **Dr Amjad Aliewi**

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The objectives of surface geophysical techniques are:

- 1. To determine indirectly the extent and the nature of the geological materials beneath the surface
  - ✓ Thickness of formations;
  - ✓ Depth of water table;
  - ✓ Location of subsurface faults;
  - ✓ Depth of the basement rocks;

2. To minimize the extent and thickness of fresh groundwater lenses in saline aquifer (water quality) or clay lenses in aquifers (lithology).

The correlation of geophysical data with well logs or test-boring data is generally more reliable than either type of information used by itself. The interpretation of physical parameters into rock type requires information from remote sensing surveys, mapping and, in particular, data from exploration drilling activities.

In geophysical techniques, rock parameters are measured as a response to energy fluxes injected into the earth. The most common geophysical techniques are:

- ✓ Geo-electrical;
- ✓ Electromagnetic;
- ✓ Seismic;

## 4.1 Surface Geo-electrical Techniques (Electrical Resistivity)

#### 4.1.1 Working Principle

- These techniques are based on the injection of an electrical current of very low frequency into the earth by means of two current electrodes (**Figure 4.1**);
- The potential differences which are created between these electrodes are measured at another pair of intermediate electrodes, the measuring or potential electrodes;
- Readings of current strength at the current electrodes, and potential differences at the measuring electrodes, and potential differences at the measuring electrodes enable us to determine rock resistivities;
- These resistivities can be related to subsurface rock types, rock water contents and groundwater quality (pore water resistivity). This information can be used to identify permeable rocks.

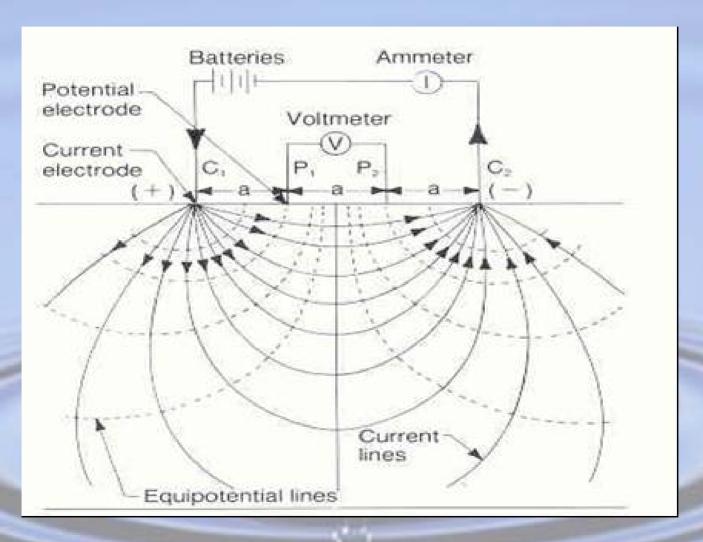


Figure 4.1 Set up for a geo-electrical measurement

#### 4.1.2 The Concept of Apparent Resistivity

When carrying out a geo-electrical measurement we do not measure the resistivities of the individual layers, but we are able to compute a so-called apparent resistivity. The apparent resistivity is in fact a combination of the resistivities of the individual layers (see **Figure 4.2**);



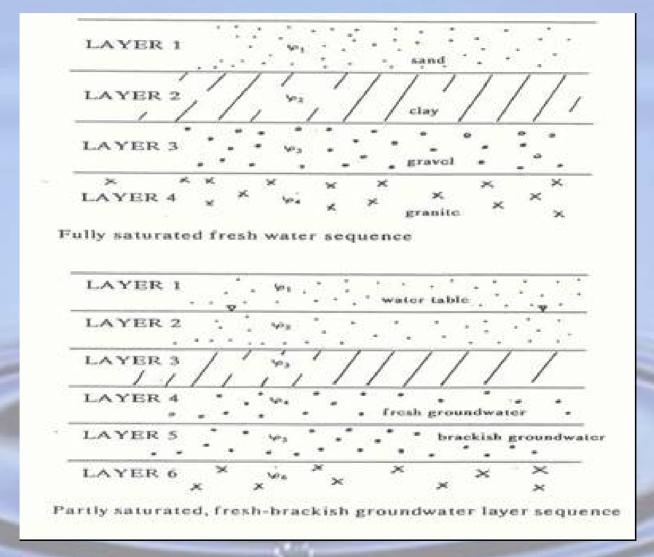


Figure 4.2 Examples of layer sequences

> The general formulation of Ohm's law is as follows:

	-dV=IxR	(1)
Where,		
dV	potential drop	(volt/m)
I	current length	(Ampere)
R	resistance	(ohm)

Imagine a single current source at land surface. Assume that the resistivities of the individual rock layers can be combined in apparent resistivities. The current (I) injected at the current sources expands itself as a semi sphere into the earth, with the atmosphere acting as a complete insulator. Figure 4.3 shows that around the source semi-spherical shells can be considered through which the current is passing at right angles.

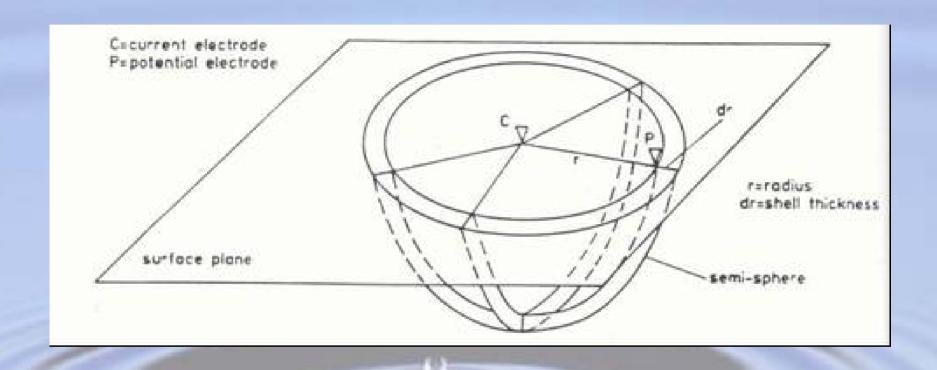


Figure 4.3 Semi-sphere around current electrode

Consider such a semi-spherical shell located at a given distance from the current source. If we consider equation 1 for the shell then the resistance (R) is proportional to the width of this shell and it is inversely proportional to the cross sectional area. The resistance is also proportional to the apparent resistivity of the medium. Thus, we can write:

$$R = \varphi_a x \frac{dr}{2\pi r^2} \tag{2}$$

Where,

 $\phi_a$  apparent resistivity  $(\Omega-m)$ 

dr width of shell (m)

r distance from shell to current source (m)

4/4

Equations (1) and (2) can be combined. This resulting expression can be written as follows:

$$dV = -I x \varphi_a x \frac{dr}{2\pi r^2}$$
 (3)

Integration of equation (3) yields for the potential at a distance (r) from the current source:

$$V(r) = \frac{I x \varphi_a}{2\pi r} \tag{4}$$

In the set up for the geo-electrical field measurement, we have two current electrodes acting as current sources. Simultaneously we apply a current strength +I at one current electrode and a current strength -I at the other electrode. This means that we have to consider the potential at a measuring electrode as generated by both current sources; the positive source and the negative source. Using equation (4) the potentials can be determined for a generalized electrode configuration (see Figure 4.4) 4/4

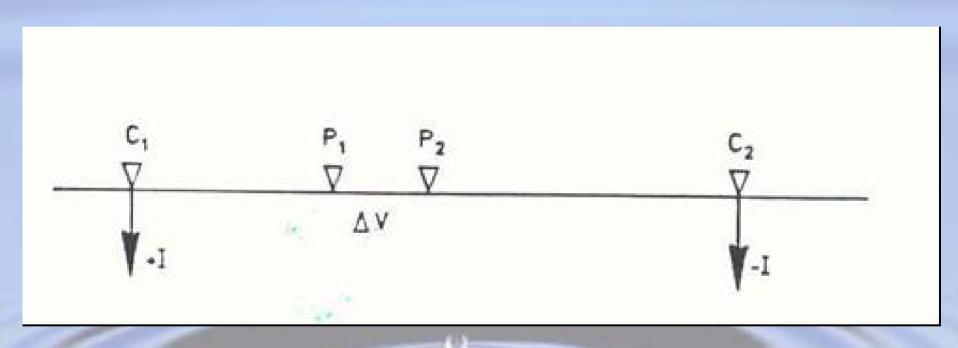


Figure 4.4 Generalized layout for a measurement

Let us denote the current electrodes by  $C_1$  and  $C_2$ , the measuring electrodes by  $P_1$  and  $P_2$  and the distances between the electrodes by  $C_1P_1$ ,  $C_2P_1$ ,  $C_1P_2$ , and  $C_2P_2$ . The potential at  $P_1$  is then:

$$V(P_1) = \frac{I x \varphi_a}{2\pi (C_1 P_1)} + \frac{-I x \varphi_a}{2\pi (C_2 P_1)}$$
 (5)

and the potential at P<sub>2</sub> is:

$$V(P_2) = \frac{I x \varphi_a}{2\pi (C_1 P_2)} + \frac{-I x \varphi_a}{2\pi (C_2 P_2)}$$
 (6)

In a geo-electrical field measurement we measure the potential difference  $(\Delta V)$  between the two measuring electrodes:  $V(P_1) - V(P_2)$ . Thus the above equations are subtracted from each other:

$$\Delta V = -I \frac{\varphi_a}{2\pi} x \left[ \frac{1}{C_1 P_1} - \frac{1}{C_2 P_1} - \frac{1}{C_1 P_2} + \frac{1}{C_2 P_2} \right]$$
 (7)

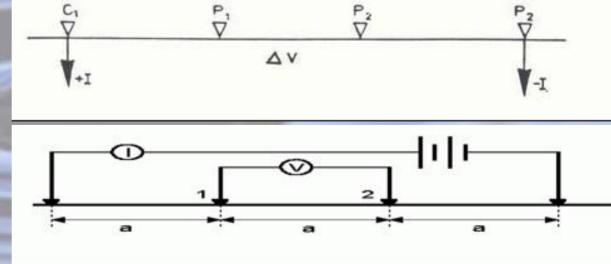
Re-arranging the terms in the above equation yields the apparent resistivity:

$$\varphi_{a} = \frac{\Delta V}{I} x \frac{2\pi}{\left[\frac{1}{C_{1}P_{1}} - \frac{1}{C_{1}P_{2}} - \frac{1}{C_{2}P_{1}} + \frac{1}{C_{2}P_{2}}\right]}$$
(8)

Figure 4.5) and 'Schlumberger' configurations (see Figure 4.6). Wenner configuration is symmetrical with the four electrodes always at equal distances from each other. The Schlumberger configuration is also symmetrical, but the distance between the measuring electrodes differs from the spacing between the measuring and current electrodes.

Figure 4.5

Wenner layout



For the Wenner spacings (see Figure 4.5)

$$C_1 P_1 = P_1 P_2 = \frac{1}{2} x C_1 P_2 = \frac{1}{2} x C_2 P_1$$
 (9)

When writing the electrode spacing in **equation 8** in terms of the spacing between the measuring electrodes,  $P_1P_2$ , then the resulting **apparent** resistivity (ohm-meter) for the **Wenner** layout can be written as follows:

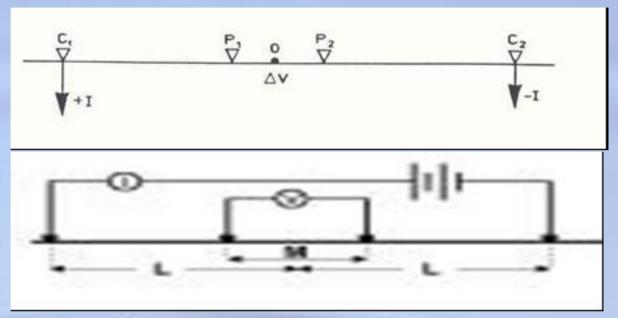
$$\varphi_a = \frac{\Delta V}{I} x 2\pi x P_1 P_2 \tag{10}$$

For the **Schlumberger** spacings (see **Figure 4.6**):

$$C_{1}P_{1} = C_{2}P_{2} = \frac{(C_{1}C_{2} - P_{1}P_{2})}{2}$$
and 
$$C_{1}P_{2} = C_{2}P_{1} = \frac{(C_{1}C_{2} + P_{1}P_{2})}{2}$$
(11)

Figure 4.6

Schlumberger layout



This expression can also be combined with **equation 8**. Expression the spacings in (8) in terms of the spacings between measuring electrodes and the current electrodes,  $C_1C_2$ , results in the following equation for the **apparent resistivity** (Ohm-meter) for the **Schlumberger** arrangement:

$$\varphi_a = \frac{\Delta V}{I} x \pi x \frac{\left[ (C_1 C_2)^2 - (P_1 P_2)^2 \right]}{4P_1 P_2}$$
 (12)

4/4

#### **4.1.3** The Variable Electrode Distance Technique

During measurement, the distances between the current and measuring electrodes are gradually increased, while the center of the layout remains at a fixed point. Various current strength and potential difference readings are taken at one location.

Apparent resistivities computed from current strength and potential difference readings can be translated into resistivities and thicknesses of individual subsurface layers.

#### **4.1.4 Field Guidelines**

- Select the area for geoelectrical surveying using the variable electrode distance technique on the basis of all existing data available (remote sensing; hydrogeological mapping and well inventories).
- For Geo-electrical techniques are used in areas of varying geologic nature. The technique is also engaged in areas of varying geological nature. The technique is also engaged in areas with consolidated sedimentary rock and in the weathered parts of metamorphic and igneous rocks. The method works best when we have:
  - ✓ Simple stratigraphical and tectonic conditions;
- ✓ Moderate or no dip of the rock layers;
- ✓ Large resistivity contrasts between subsurface layers

Plot the measurements on section lines which are perpendicular to the main strike direction of the subsurface rock layers. The distance between section lines, and between the individual measurements depends on the required amount of detail. Distances between measurements are 50-1000 m.



Extend the electrode spacing along a straight line perpendicular to the selected section lines. I and  $\Delta V$  are measured from each electrode spacing, while the center of the measurement line (the axes through the electrodes) remains at a fixed position. At small electrode spacing the depth penetration of the electrical current is small and the potential difference readings relate to the resistivity of the first rock layer. When we proceed, the readings at larger spacings relate to the deeper layers. We will continue until the maximum electrode spacing is reached (as a "rule of thumb" we can take that the maximum spacing between current electrodes is equal to (3-4) times the required investigation depth). However, the final decision on the completion of the measurements should be taken in the field itself and depends on the shape of the (apparent) resistivity curve and on the smoothness of this curve (only smooth curves lend themselves to interpretation).

 $\triangleright$  Selection of layout: In the **Wenner** set-up the electrode spacing  $C_1P_1$ , P<sub>1</sub>P<sub>2</sub>, and P<sub>2</sub>C<sub>2</sub> remain constant, but this also implies that after each reading all four electrodes have to be brought to new, larger spaced positions. In the **Schlumberger** arrangement the electrode spacings C<sub>1</sub>P<sub>1</sub>,  $C_2P_2$  are identical but differ from  $P_1P_2$ . During the measurement the  $P_1P_2$  is kept constant during a series of readings for increasing current electrode spacing. Then the P<sub>1</sub>P<sub>2</sub> is increased and again kept constant while the next set of readings for increasing current electrode distances C<sub>1</sub>C<sub>2</sub> is taken. On the field curve we can distinguish the various sets of readings for typical P<sub>1</sub>P<sub>2</sub> values as "branches" which partly overlap each other.

 $\triangleright$  In Wenner surveys  $\triangle V$  can usually be measured somewhat more accurate than in Schlumberger surveys where P<sub>1</sub>P<sub>2</sub> is relatively small as compared to the current electrode spacing. The Schlumberger set up has as its main advantage that lateral changes in the subsurface geology can better be detected from shifts in the various field curve branches. The interpretation of Schlumberger field curves with curve matching techniques is also more accurate. Wenner surveys may be somewhat faster than the Schlumberger surveys, but the Wenner survey usually requires one or more laborer to replace the electrodes.

Taking the measurements: select the electrode spacings in such a way that half the current electrode spacing, C<sub>1</sub>C<sub>2</sub>/2, plot more or less equidistantly on double-logarithmic paper. Measuring tapes may be rolled out to mark the sites for the electrodes or marks may be made on the cables. During the measurement, determine the apparent resistivity for each electrode spacing from the recorded  $\mathbf{I}$  and  $\Delta \mathbf{V}$  (or their ratio). Multiply ΔV/I with a **geometrical factor G** (equal to that part of equation 10 or 12 describing the electrode spacings) will give us the value for the apparent resistivity.

Plot the  $\phi_a$  values for the production of a field curve straightaway on log-log paper.  $\phi_a$  values are usually plotted along the y-axes and the corresponding  $C_1C_2/2$  along the x-axes. Direct plotting helps identifying errors become in the field, and not later in the office. An example of a typical Schlumberger configuration is presented in **Table 4.1** 



Table 4.1 Example of a typical Schlumberger configuration

P <sub>1</sub> P <sub>2</sub> /2	C <sub>1</sub> C <sub>2</sub> /2	G	P <sub>1</sub> P <sub>2</sub> /2	C <sub>1</sub> C <sub>2</sub> /2	G
0.5	1.5	6.28	10	25	82.8
0.5	2.5	18.8	10	30	126
0.5	4	49.5	10	40	235
0.5	6	112	10	50	377
0.5	8	200	10	60	549
0.5	10	313	10	75	867
0.5	12	451	10	100	1554
0.5	15	706	25	75	314
4	12	55.7	25	100	589
4	15	82	25	125	942
4	20	151	25	150	1374
4	25	239	25	200	2473
4	30	347	25	250	3886
		-	25	300	5616

#### 4.1.5 Principles of Resistivity Interpretation

- In the field we measure **I** and **ΔV** for various electrode spacings. Then apparent resistivity values are computed using **equations 11 and 12**. We end up with a whole series of apparent resistivities for a range of electrode spacings. The next step is to translate the values of apparent resistivity into layer resistivities  $\varphi_1$ ,  $\varphi_2$ ,  $\varphi_3$  etc. and into layer thicknesses  $h_1$ ,  $h_2$ ,  $h_3$  etc.
- This interpretation is done by means of curve matching techniques which are valid for horizontally stratified earth layers. Field curves showing apparent resistivities against current electrode spacings are matched with master curves which are computed from mathematical expressions. In case field and master curves fit, the layer resistivities thickness at a measurement location are similar to those used for the computation of the master curves.

- Traditionally sets of master curves which were determined from the mathematical expressions were drawn on paper, and curve matching with field curves was done manually. Nowadays the computation and presentation of 'master' curves, and the storage and presentation of the field curves is largely done on the personal computer.
- Mathematical Expressions: for the case of two layers the final result of the derivation for the mathematical expression will be presented. The equation relates apparent resistivities to resistivities of the first and second layer, the thickness of the first layer, and to current electrode spacings. The deepest layer, which in case is the second layer, is always assumed to be of infinite thickness (see **Figure 4.7**). Also, note that an electrode configuration following the Schlumberger arrangement has been assumed. The expression with a written on the left hand side in equation 13.

$$\frac{\varphi_{a}}{\varphi_{1}} = 1 + 2x \sum \frac{\left(\frac{C_{1}C_{2}}{2h_{1}}\right)^{3} x K_{12}^{n}}{\left[\left(\frac{C_{1}C_{2}}{2h_{1}}\right)^{2} + 4n^{2}\right]^{1.5}}$$
(13)

Where,

$$K_{12}$$
  $(\phi_2-\phi_1)/(\phi_2+\phi_1)$   
 $h_1$  thickness of first layer (m)  
 $n$  n-times of mirroring

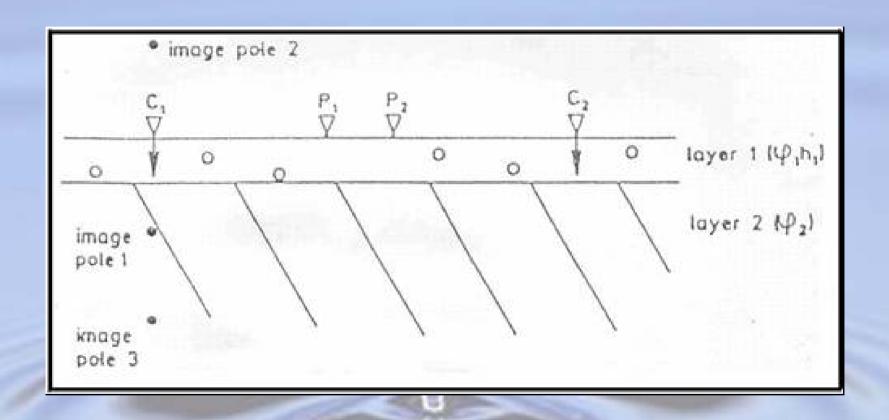
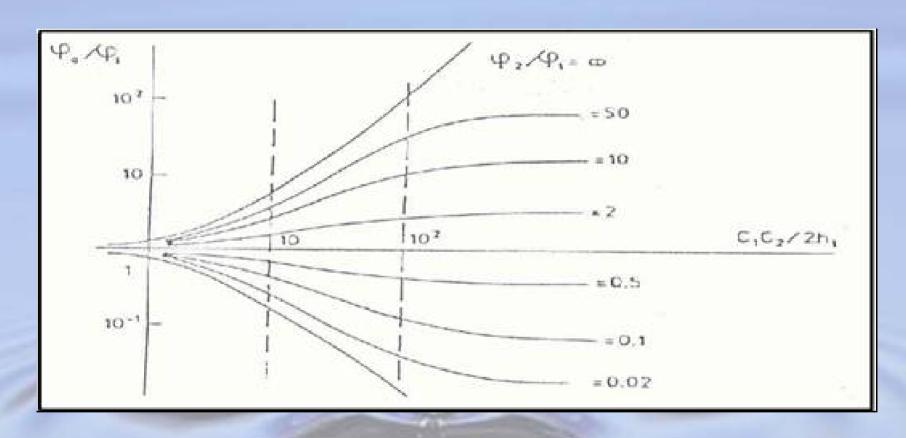


Figure 4.7: Image poles in a two-layer case

For small current electrode spacings, the apparent resistivity approaches the resistivity of the first layer. On the other hand, for very large electrode spacings, the apparent resistivity will then be equivalent to the resistivity of the second layer.

Two layer master curves: equ.13 shows that hundreds of master curves could be drawn up for as many combinations of selected values for the layer resistivities  $\phi_1$  and  $\phi_2$ , and the thickness of the first layer  $h_1$ . By plotting on double logarithmic paper the ratios of the apparent resistivity values and the resistivity of the first layer, and the ratio of half the current electrode distance and the thickness of the first layer (C<sub>1</sub>C<sub>2</sub>/2h<sub>1</sub>), the master curves can be reduced to a set that fits on one sheet of paper. Figure 4.8 presents schematically the set of two-layer master curves. Note that the first layer and the second layer are reflected respectively by the asymptotic end at the left hand side and the right end side of the curve.

Figure 4.8 shows that the two-layer master curves have been drawn up for various ratios of  $\phi_2/\phi_1$ . Field curves are also plotted on double logarithmic paper, but on the Y-axes the unit is  $\varphi_a$  and on the X- axes we assume a unit of  $C_1C_2/2$ . Thus, in case a field curve fits to a two-layer master curve, constant shift between X axes and the Y-axes of both curves can be observed: in the Y direction, the shift is  $\varphi_1$  and in the X direction, the shift is h<sub>1</sub>. By reading off the shifts in the Y and X direction between fittings field and master curves, the two-layer master curves can be used for the determination of the resistivity  $\phi_1$  and the thickness  $h_1$  of the first layer. The resistivity of the second layer can be computed from the ration  $\Phi_2/\Phi_1$ 



**Figure 4.8: Two layer Master Curves** 

Three layers master curves: master curves for the three-layer case cannot be presented in a single diagram. Sets of three-layer master curves can be classified according to their shape. Figure 4.9 presents examples of each of the four types of three-layer master curves. In these curves the first layer is reflected in the left hand side of the curve; the middle layer is reflected in a maximum, minimum or a distinctive change in slope in the ascending and descending segment somewhere in the middle of the curve, and the third layer corresponds to the right hand side of the curve.

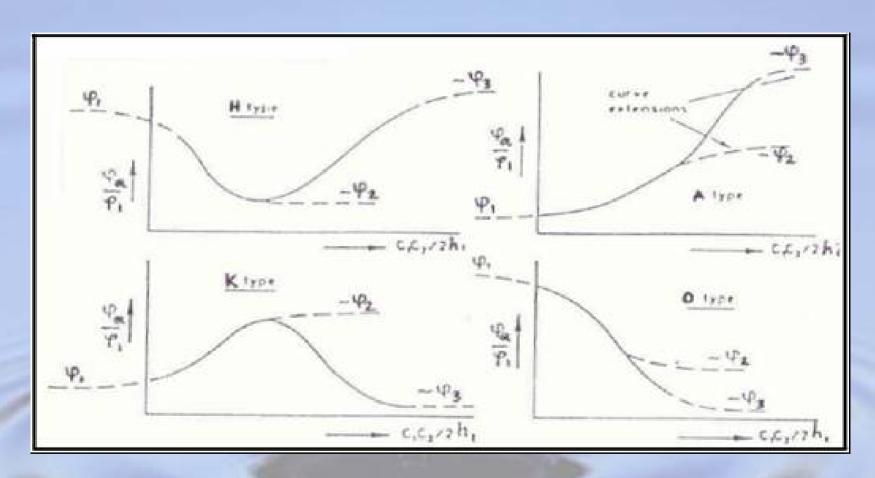


Figure 4.9: Types of three Layer Master Curves

#### **4.1.6 Porewater Resistivity**

- The resistivity of a subsurface layer (formation resistivity) depends on:
- ✓ Porewater resistivity;
- ✓ Rock type pore space (porosity);
- ✓ Water content of the rock.

The porewater resistivity is determined by the properties of the groundwater in pores, joints, fractures and solution holes contained in rock. Properties include the concentration of total solids in solution, the type of ions dissolved and water temperature. Therefore, the porewater resistivity is also a measure of the groundwater quality. The influence of the concentration of total dissolved solids is most influential. The higher the concentration of total dissolved solids, the higher is the water conductivity, and the lower is the porewater resistivity. This relationship is shown in Figure 4.10, where the concentration of two of the most common solids dissolved in groundwater (sodium chloride NaCl, and sodium bicarbonate NaHCO<sub>3</sub>), are set out against the water conductivity and the water resistivity of the solution.

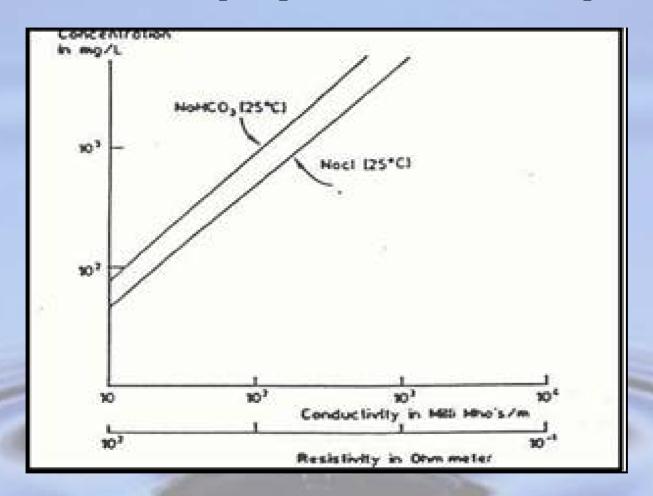
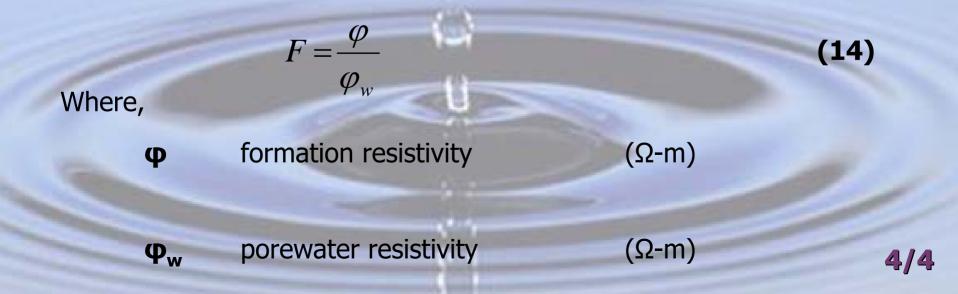


Figure 4.10: Relation between concentration and resistivity

#### 4.1.7 Formation Factor

For saturated conditions, the formation resistivity is made up of the resistivity of the porous rock and the porewater resistivity. The resistivity of the rock is usually much larger than the resistivity of the porewater. Thus, the formation resistivity is generally larger than the porewater resistivity. The formation factor F is defined by:



The formation factor can be related to rock type characteristics and rock porosity. The expression which is only valid for sedimentary rocks is as follows:

$$F = C x \theta^{-m} \tag{15}$$

Where,

- **\theta** porosity of the rock
- **C** tortuosity depending on the mineralogy of the rock and the angularity of the grains; for rounded grains C~1.
- **m** Cementation factor which ranges from 1.3 for loose sediment to 1.95 for well cemented formations.

The formation factor for unconsolidated sediments ranges from about 1 to 6 (e.g. for clays F is in the 1-2 range, while for coarser sands, F values in the order of 5-6 are common). **Table 4.2** gives a summary of formation factors common for unconsolidated sediments. In the more consolidated sediments the porosities are usually lower and formation factors for these rocks tend to be higher.



**Table 4.2:** formation factors for some unconsolidated sediments

Lithology	F		
Gravel	7.5		
Coarse sand and gravel	6		
Coarse san	5		
Medium sand	4.2		
Fine sand	3.5		
Clayey sand	<2.5		

#### **4.1.8 Hydrogeological Interpretation Procedures**

- The interpretation means in the first place that we will have to associate the formation resistivities (rock layer resistivities) determined at geo-electrical measurement sites with rock types, rock water contents and porewater resistivities. Follow the **resistivity** allocation and correlation procedure:
- Allocation is the assignment of rock type and formation factor, rock water content, and porewater resistivity or conductivity value interpreted at an individual geo-electrical measurement site. The formation which is compiled on the so-called calibration tables should be used to complete these activities. Preferably, calibration tables are prepared on the basis of data collected during an exploration drilling programme.

Correlation is the activity whereby the interpreted formation resistivities at the various individual measurement sites are compared with each other. Correlation may first be carried out on the basis of resistivity values alone and then be finalized after rock characteristics have been assigned (see above). This can best be carried out by setting up cross sections along the lines of geo-electrical measurement sites and any exploration wells on these lines. Subsurface layers with similar characteristics on these sections may be connected with each other, presenting an excellent view of the (hydro)geological conditions within an investigated area.

See Table 4.3 as an example for calibration of porewater resistivity

Table 4.3: Example of a calibration table (the Rada

Area in Yamen)

Formation φ (Ω-	Rock Type	Water	Porewater φ
m)		Content	(Ω-m)
< 10 30 - 70 30 - 100 80 - 200 > 1000 > 1000	Alluvial sand Alluvial sand Weathered basement Sandstone Alluvial sand Basement gneiss	Saturated Saturated Saturated Saturated Unsaturated Dense rock	< 3.3 (brackish) 10 – 25 (fresh) 10 – 25 (fresh) 10 – 25 (fresh)

#### 4.1.9 Interpretation Hazards

- The use of allocation and correlation techniques for geoelectrical interpretation may be complicated or tricky for a number of reasons. First, the formation resistivities at the measurement sites may be considerably higher or lower than the range of values offered by the calibration table.
- Secondly, it is normally assumed that in case the formation resistivity values at the measurements sites and at the exploration, drilling sites are similar, the  $\phi_w$  and F values are also similar. This is not always correct. Formation resistivities in an investigation area would not show any spatial variation as long as the product  $[Fx \phi_w]$  is constant. The case may present itself that at a geo electrical measurement site this product is indeed the same as at exploration drilling sites, but that nevertheless, the F and the  $\phi_w$  are quite different. We are then inclined to make an interpretation error. Only when we have a good perception of the area interpretation errors like these can, be avoided.

## **4.1.10** Data Interpretation for Constant Electrode Distance

For the Wenner arrangement (constant electrode distance survey), the apparent resistivity values for the successive measurement positions can be calculated from Eq. 11. For reconnaissance, surveying the apparent resistivities can be plotted on a topographical or geological map. Contour lines (iso-resistivity lines) may be drawn on these maps and sub-areas with typical apparent resistivity values can be delineated. For "discontinuity" surveying a plot may be made showing distances to the measuring points from the start of the section line (on x axis) against the corresponding apparent resistivity values (on y axes).

#### **SESSION 10**

# GROUNDWATER EXPLORATION III



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The hydrological interpretation based on measurements following the constant electrode distance technique is a rather qualitative interpretation. For the case of reconnaissance surveying the rock type, the rock water content or the porewater resistivity can also be estimated for a selected investigation depth. Only estimates are possible.

Figure 4.11 shows an apparent resistivity map for the North of Surinam gives details. The coastal groundwater basin underlying the area consists of unconsolidated sediments up to several hundreds of meters of unconsolidated sediments up to several hundreds of meters below ground surface. The resistivity values and iso-resistivity lines which are shown on the map correspond with an investigation depth of 150 to 200 m below ground surface. The interpretation is as follows:

The sub-area near to the coastline with relatively low formation resistivities in the order of **2.5 to 5**  $\Omega$ -**m** point to low porewater resistivities. This correlates with the occurrence of brackish to saline groundwater at the elected investigation depth.

For similar depths ranges, the higher resistivities in the order of  $\bf 6$  to  $\bf 8$   $\bf \Omega$ - $\bf m$  for the sub-areas farther inland represent fresh to brackish groundwater.

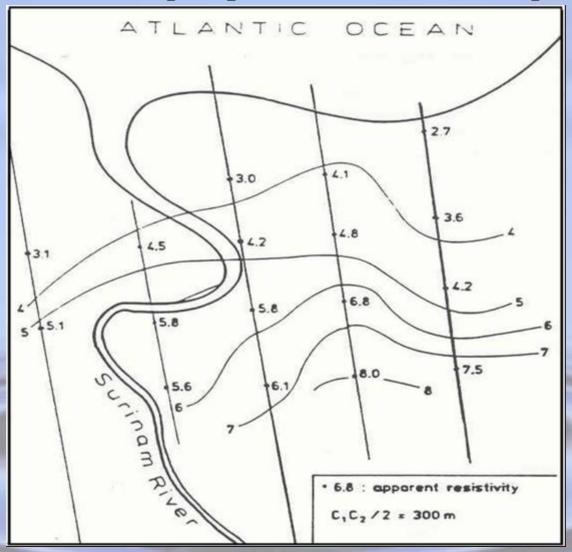


Figure 4.11: Map with resistivities: North of Surinam

When surveying for "discontinuities" the hydrogeological interpretation is also largely qualitative. For example, fault zones usually have higher water contents than the surrounding rock. This is reflected in a low apparent resistivity. Thus, a fault can be detected by low apparent resistivity values in a measurement series. Let us consider another example of a "discontinuity": a dolerite dike. Dikes may be associated with a low formation factor due to the presence of conductive iron-containing minerals. This will also be reflected in low apparent resistivity values which will be indicated when surveying across the dike. We can conclude from the above that an interpretation of apparent resistivity data cannot stand alone: they have to be considered in combination with data from other sources.

#### 4.1.11 CASE STUDY (Driscoll, pp 179-181)

- A consultant was retained by a developer to locate suitable groundwater supply for a proposed mobile home park.
- A test well drilled on the northwest potion of the property to a depth of 250 ft, encountered about 50 to 60 ft of fine sand. The yield was about 100 gpm, much less than the developer required. The consultant recommended that a surface resistivity survey be conducted over the entire parcel to define the most promising area for another well.

A resistivity survey consisting of 44 stations was laid out on a grid shown in **Figure 4.12**. Earth resistivity was taken with a Wenner array using 10, 20, 40, 60, 80, 120 and 160 ft a-spacing readings. These data enabled the consultant to construct an apparent resistivity/depth profile at each location. Cross sections of corrected resistivity were plotted in **Figure 4.13**. The profiles were contoured and then studied to determine whether any particular depth intervals displayed high values of resistivity which would indicate the presence of saturated sand and gravel lenses.

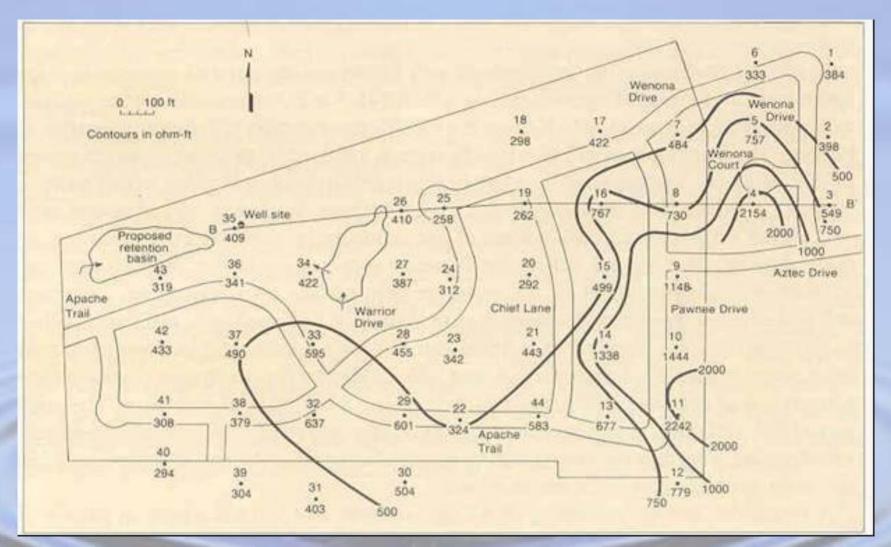
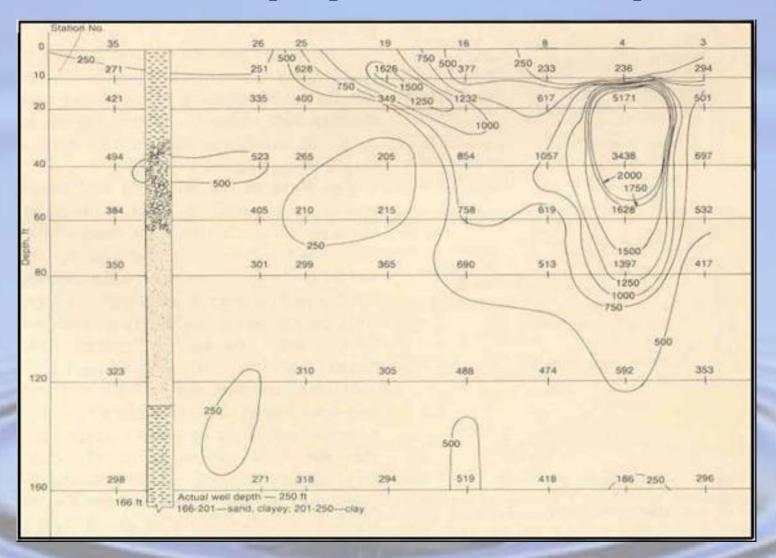


Figure 4.12: Resistivity layout for the proposed mobile home park.

Values for the 40, 60, and 80 ft readings have been averaged 4/4



**Figure 4.13**: Profiles, or cross sections, of corrected resistivity. The readings indicate a thick sequence of saturated sand and gravel near the eastern border of the site.

Interpretation of resistivity values obtained from the survey indicate that aquifer conditions would be much more promising toward the eastern end of the property. Test drilling was recommended along the line of stations 8, 9, and 10. Ideally, drilling should have occurred along the line of stations 4, 5 and 6 but this area had already been developed with homes (see **Figure 4.14**).



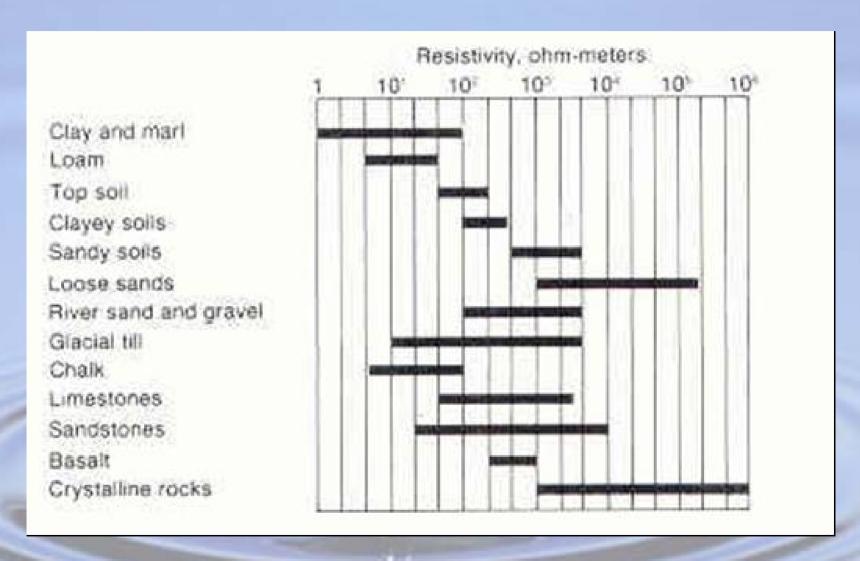


Figure 4.14: Ranges of resistivity values for various earth materials

4/4

Subsequently, a 12-in well was installed to a depth of 90 ft at the selected location. The boring encountered sand and gravel from a depth of about 5 ft to the bottom of the boring at 19 ft. during a 24 hour aquifer test, the well was pumped at 1,250 gpm, the specific capacity was 70 gpm for 100 days of continuous pumping which far exceeded the short term 100 gpm yield of the original test well a few hundred feet to the West.



# 4.2 Surface Electro-Magnetic Techniques 4.2.1 Working Principle

Primary electro-magnetic fields are generated by a transmitter at land surface. They induce currents at subsurface conductors which include rock types of a low resistivity. The induced currents produce a secondary electro-magnetic field that differs in magnitude and orientation, and in phase from the primary field. A recover measures the resulting total field. The principle is illustrated in **Figure 4.15**.

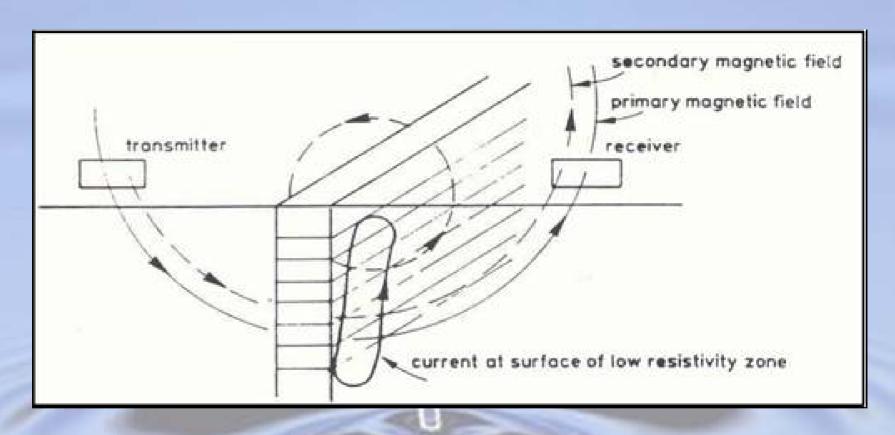


Figure 4.15: Principles of electro-magnetic techniques

The receiver measures the phase or the resulting primary plus secondary field (total field). The phases of the individual primary and secondary fields can be determined from these measurements. We will find that the phase of the secondary field generated by the subsurface conductor differs from the phase of the primary field. The better the conductor the more lags the phase of the secondary field behind the phase of the primary magnetic field. For very good conductors the phase of the secondary field may even lag 180 degrees behind the phase of the primary field. For poor conductors the phase difference between primary and secondary magnetic fields is usually in the order of 90 degrees (see Figure 4.16).

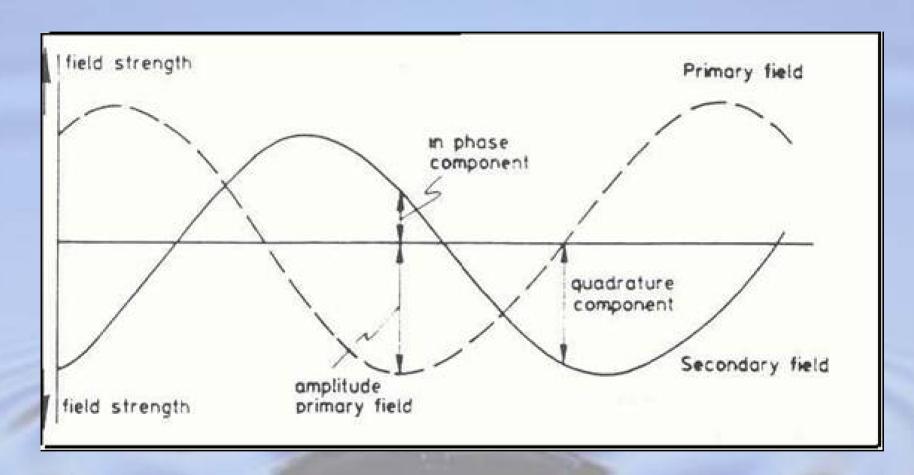


Figure 4.16: primary and secondary magnetic fields

Field strengths for the secondary field can be computed from the measurements recorded by the receiver. These field strengths can be used to find implicit values for the resistivities of subsurface conductive rock layers.

## **4.2.2 Variable Electrode Distance Geo-electrical Technique**

#### **ADVANTAGES**

- It can be used for the exploration of underground in a large variety of areas with diverse geological conditions.
- It is still the superior surveying techniques when information on the individual subsurface rock layers is required.
- The time needed for surveying and interpretation can be shortened.

#### **DISADVANTAGES**

- A large entry resistance at the current electrodes (very dry conditions) may jeopardize the measurements. Mineralized water is usually added to improve conditions.
- In areas with very low layer resistivities (brackish to saline groundwater), the potential differences to be measured may be too small and cannot be accurately measured. Working with larger currents may help.
- The method is still time consuming and expensive. In comparison with other geophysical techniques survey time may be 3 to 4 times as long.

#### **4.2.3 Electro-Magnetic Techniques**

These are often considered compatible with Geo-electrical techniques. In particular electro-magnetic surveys are thought to be in the same league as the Geo-electrical surveys following the constant electrode distance arrangement. Engaged in reconnaissance surveying, both techniques can be used to obtain a quick impression of the resistivities of the subsurface layers in an area. Also, both techniques are well suited for tracking down vertical or steeply dipping "discontinuities" such as fault zones or intrusive dykes and sills in hard rock areas.

#### **ADVANTAGES**

- Electro-magnetic surveying is faster than Geo-electrical surveying following the constant electrode distance technique.
- Electro-magnetic surveying is relatively inexpensive. Capital investment for some of the instrument is similar to the acquisition cost of Geoelectrical equipment. The cost gain is in time and in labor. For electro-magnetic surveying one or two men are usually required, while in Geoelectrical surveying at least three men will have to be employed (see **Figure 4.17**).



Figure 4.17: Hand-carried terrain conductivity devices use electromagnetic waves to measure the conductivity of earth materials. Direct contact with the ground is not required during data gathering. Thus, subsurface information can be obtained quickly in both highly urbanized and rural environments.

- In case surface layers with a sufficiently high resistively are present then the electro-magnetic method is ideally suited to unravel conductive rock layers, or bodies etc at larger depths. This is done for relatively small transmitter-receiver spacings. If we employ Geo-electrical techniques following the constant electrode distance method large electrode spacings are needed and more geological details may be lost. Such detail could have been detected if an electro-magnetic survey would have been set up.
- Electro-magnetic surveying may work better in case we deal with resistive surface layers. The magnetic fields that we use in electro-magnetic surveying are by no means hampered by such layers. On the other hand, electric currents which we use in Geo-electrical surveying may be obstructed due to large entry resistance.

#### **DISADVANTAGES**

Electro-magnetic surveying is severely hindered by the presence of man-made conductors, e.g. power lines, buried pipes, cables and wire fences.

In case surface layers have a low resistivity then the electro-magnetic response tends to be primarily generated by these layers. There will be an inadequate response of any deeper rock layers, or these layers may not even be detected.

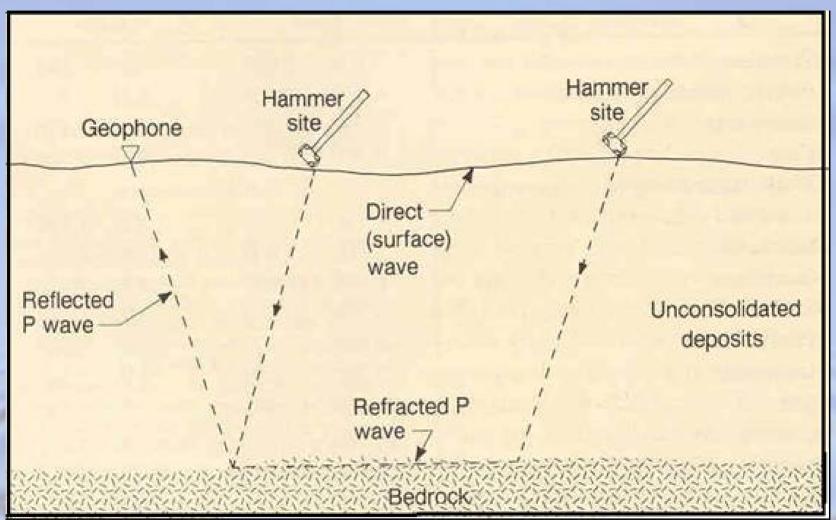
Interpretation may be carried out in a qualitative way. There is no direct information on rock properties such as apparent rock resistivities.

## 4.3 Seismic Refraction Method 4.3.1 Working Principle

- The seismic refraction method is based on the fact that elastic waves travel through different earth materials at different earth velocities. The denser the material, the higher the wave velocity.
- The waves are called elastic because as the waves pass a point in the rock, the particles are momentarily displaced or distorted but immediately return to their original position or shape after wave passes;

- Three types of waves can be created: Compressional waves (P), Shear waves (V), and surface waves. Compressional waves are the first to arrive at the geophones and therefore are the most useful in seismic surveys;
- In general, the higher the density and elasticity of the rock unit, the faster the P wave will be transmitted. The velocity is much less and the energy is dissipated more quickly if the material is unconsolidated or poorly consolidated.

Three distinct paths are taken by compressional waves in the ground: direct, refracted and reflected (see **Figure 4.18**). A single seismic impulse can be recorded as three separate arrivals at the geophone. In practice, however, only the first arrival can be readily recognized.



**Figure 4.18:** Waves from a seismic disturbance can travel as surface, reflected, and refracted waves. In water well exploration, analyses of refracted and reflected waves can determine the depth to bedrock at a potential drilling site

- When elastic waves cross a geological boundary between two formations with different elastic properties, the velocity of wave propagation changes and the wave paths are refracted.
- Seismic methods use artificially seismic waves traveling through the ground. By studying the arrival times of seismic waves at various distances from energy source, the depth to bedrock can be determined.
- These methods are useful in determining depth to bedrock, depth to water table and in some cases general lithology.

- Seismic refraction method is used to determine the thickness of unconsolidated materials overlying bedrock. The loose material transmits seismic waves more slowly than consolidated bedrock. By studying the arrival times of seismic waves at various distances from energy source, the depth to bedrock can be determined.
- The energy source can be a small explosive charge set in a shallow drill hole. One or two sticks of dynamite are sufficient for depths to bedrock in excess of 30 to 50 m.
- The seismic wave is detected by geophones placed in the earth in a line extending away from the energy source. Waves initiated at the surface and refracted at the critical angle by a high-velocity layer at depth will reach the more distant geophones more quickly than waves that travel directly through the low-velocity surface layer.

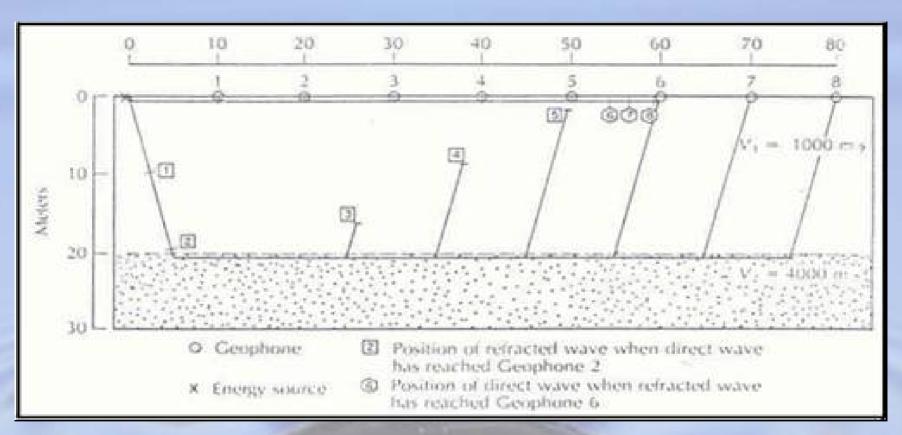
#### 4.3.2 Interpretation

- Each geological formation has a characteristic seismic velocity that affects arrival time. Some representative seismic velocities are given in **Table 4.4**
- A seismograph records the travel time for the wave to go from energy source (short point) to geophone. This time should be plot against distance from shot point to geophone;
- The most difficult problem with the reflection method is that the reflected wave is never the first to appear on the seismic record. Therefore, on an ordinary receiving device its arrival is almost impossible to recognize among the multitude of other wave arrivals. This problem can be overcome by using signal enhancement, which permits the operator to separate the primary reflected wave from others.

**Table 4.4**: Approximate range of velocities of compressional waves (P) for representative materials found in the Earth's crust

Material	Velocity*	
	Ft/sec	m/sec
Weathered surface material	1,000 - 2,000	305 – 610
Gravel, rubber, or san (dry)	1,500 – 3,000	457 - 915
Sand (wet)	2,000 – 6,000	610 – 1,830
Clay	3,000 – 9,000	915 – 2,740
Water (depending on temperature and salt	4,700 – 5,500	1,430 – 1,680
content	4,800 – 5,000	1,460 – 1,520
Sea water	6,000 – 13,000	1,830 – 3,960
Sandstone	9,000 – 14,000	2,740 – 4,270
Shale	6,000 – 13,000	1,830 – 3,960
Chalk	7,000 – 20,000	2,130 - 6,100
Limestone	14,000 – 17,000	4,270 -5,180
Salt	15,000 – 19,000	4,570 -5,790
Granite	10,000 – 23,000	3,050 - 7,010
Metamorphic rocks	12,050	3,670
Ice		
* The higher values in a given range are usually obtained at depth.		

Figure 4.19 illustrates the travel paths of compressive seismic waves traveling through a two-layer earth. The seismic velocity in the lower layer is greater than that in the upper layer. As the energy travels faster in the lower layer, the way passing through it gets ahead of the wave in the upper layer. At the boundary between the two layers, part of the energy is refracted back upward from the lower-layer boundary to the surface;



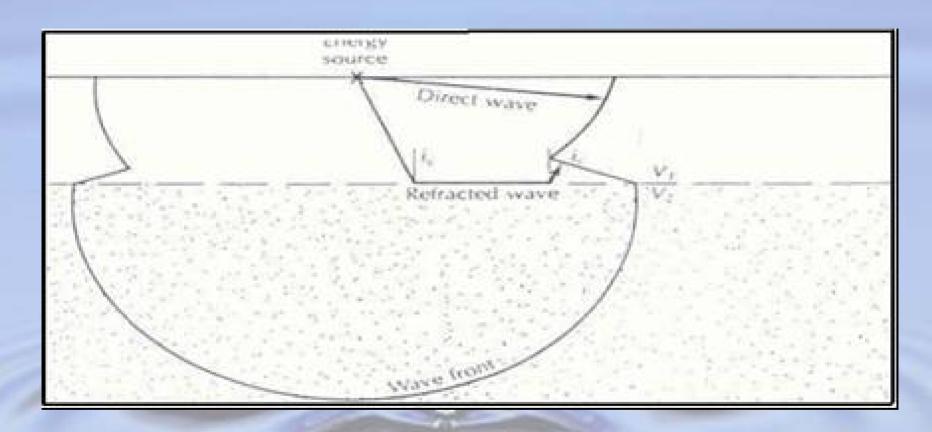
**Figure 4.19**: Travel paths of a refracted seismic wave and a direct wave. The direct wave will reach the first five geophones first, but for the more distance geophones the first travel is from a refracted wave. Numbers inside symbols refer to distances traveled by wave paths going toward the indicated geophone.

The angle of refraction of each wave front is called the critical angle  $i_c$ , and is equal to the arc sin of the ration of the velocities of the two layers:

$$i_c = \sin^{-1} \frac{V_1}{V_2}$$
 (16)

Figure 4.20 illustrates a wave front and the path of the refracted energy that travels along the lower-layer boundary. A direct wave in the upper layer is also shown.

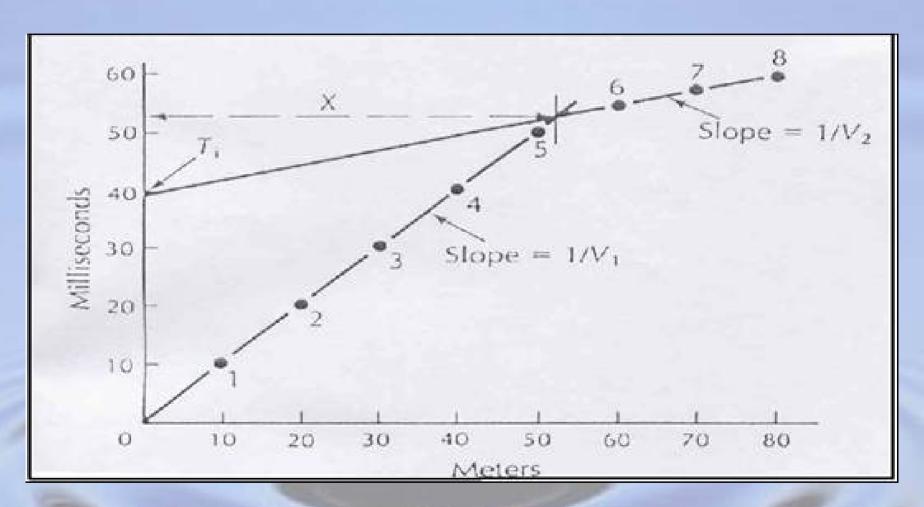
If  $V_2 < V_1$  then the wave will be refracted downward and no energy will be directed upward. Thus the refraction method will show higher-velocity layers but no lower-velocity layers that are overlain by a high-velocity layer.



**Figure 4.20**: A seismic wave front at a given time after a charge is detonated

Energy travels directly through the upper layer from the source to the geophone. This is the shortest distance, but the waves do not travel as fast as those traveling along the top of the lower layer. The latter go farther, but with a higher velocity. Figure 4.19 shows the positions of waves traveling to each geophone. Geophones 1 through 5 first receive waves that have traveled through only the upper layer. The sixth and succeeding geophones measure arrival times of refracted waves that have gone through the high-velocity layer as well. The figure shows the position of the trailing wave front at each time the leading front reaches each geophone;

A graph is made of the arrival time of the first wave to reach geophone versus the distance from the energy source to the geophone (travel-time or time-distance curve). **Figure 4.21** shows the time-distance curve for the shot in **Figure 4.19**. The reciprocal of the slope of each straight-line segment is the apparent velocity in the layer through which the first arriving wave passed. The slope of the first segment is 10 milliseconds per 10 m so that the reciprocal is 10 m per 10 ms or 1000 m/s.



**Figure 4.21**: Arrival time-distance diagram for a two-layered seismic problem.

Numbers refer to geophones in Figure 4.19.

The projection of the second line segment backward to the time-axis (X=0) yields a value known as the intercept time,  $T_i$ . As shown in **Figure 4.21**,  $T_i$  is 39 ms and X=52 m.

The depth to the lower layer Z, is found from:

(17) 
$$Z = \frac{T_i}{2} \frac{V_1 V_2}{\sqrt{V_2^2 - V_1^2}}$$

The depth to the lower layer can be also found from the equation:

$$Z = \frac{X}{2} \sqrt{\frac{V_2 - V_1}{V_2 + V_1}}$$
 (18)

where X is the distance from the shot to the point at which the direct wave and the refracted wave arrive simultaneously. This is shown in Figure 4.21 as the x-axis distance where the two line segments cross.

A more typical case in the hydrogeology is a three-layer earth, the top layer being unsaturated, unconsolidated material. In the next layer below the water table, the unsaturated deposits are saturated, which yield a higher seismic velocity. The third layer is then bedrock. Under such conditions the seismic method can be used to find the water table.

The three-layer seismic case with  $V_1 < V_2 < V_3$  is shown in **Figure 4.22**. The first arriving waves show three line segments. The reciprocal of the slope of each line is the seismic velocity of the respective layers. The intercept time for each of the two deeper layers is the projection of the line segment back to the time-axis. Indicated on the Figure is the distance X<sub>1</sub>, from the shot to the point at which waves from layers 1 and 2 arrive simultaneously and the distance  $X_2$ , to the point at which waves from layers 2 and 3 arrive simultaneously. The thickness Z<sub>1</sub> of layer 1 is found from the values of  $V_1$  and  $V_2$  and either  $T_{i1}$  or  $X_1$  using equation 17 or **18**. the thickness of the second layer  $Z_2$  is found from:

$$Z = \frac{1}{2} \left[ T_{i2} - 2Z_1 \sqrt{\frac{V_3^2 - V_1^2}{V_3 V_1}} \right] x \left[ \frac{V_2 V_3}{\sqrt{V_3^2 - V_2^2}} \right]$$

(19)

4/4

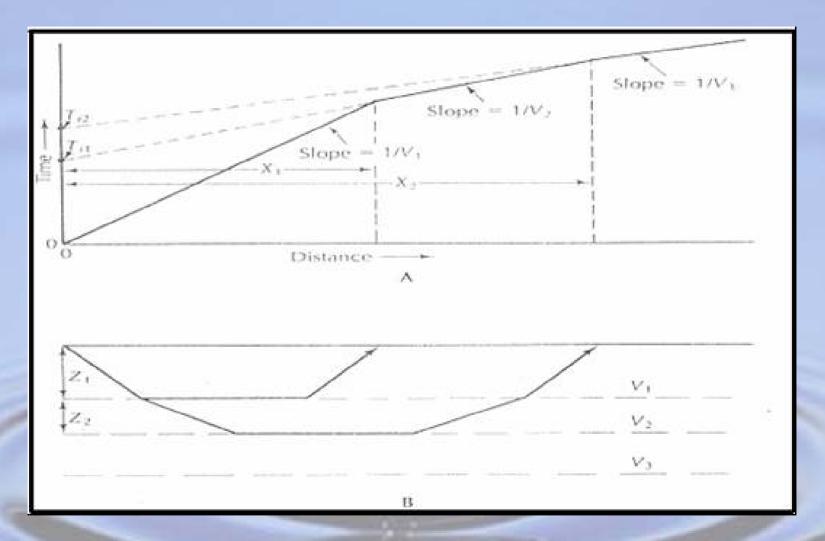
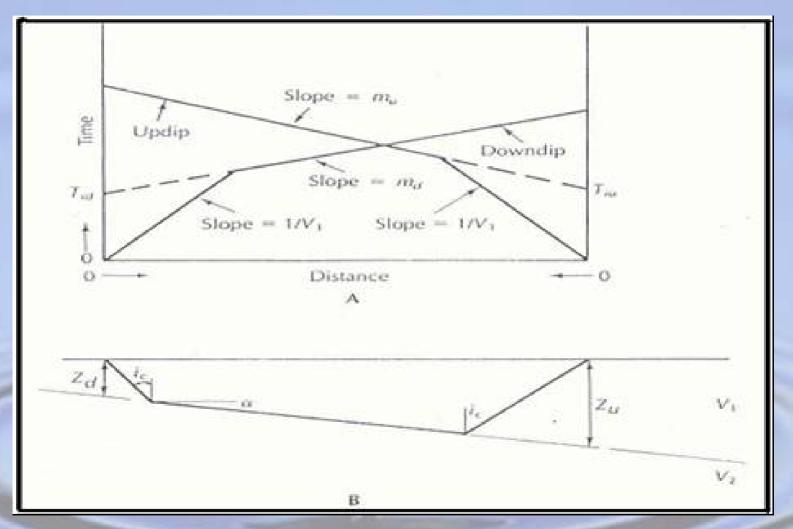


Figure 4.22: A. Diagram of arrival time versus distance for a three-layered seismic problem. B. Wave path for a three-layered seismic problem 4/4

- The velocities computed from the reciprocals of the slope are called apparent velocities. If the lower layer is horizontal, they represent the actual velocity.
- If the lower layer is sloping, the arrival time for a shot measured down slope will be different from one measured upslope. Seismic lines are routinely run with a shot at either end, so that dipping beds can be determined.
- Time-distance curves for a dipping stratum are shown in **Figure 4.23**, with travel times measured from shots at either end of the line. The upper layer is unaffected by the dip of the lower bed, so that the reciprocal of the slope of the first line segment is  $V_1$ . in order to find the values of  $V_2$  and the depth to the bedrock at the undip end of the line  $Z_d$ , as well as at the downdip end  $Z_{IJ}$ , a complex series of computations must be made.



**Figure 4.23**: **A.** Diagram of arrival time versus distance for two-layered seismic problem with a sloping lower layer. **B.** Wave path for the preceding problem **4/4** 

The slope of the second line segment of the downdip line  $m_d$ , and the slope of the second line segment of the updip line is  $m_u$ . The value of the angle refraction  $i_c$ , is found from:

$$i_c = \frac{1}{2} \left[ \sin^{-1} V_1 m_d + \sin^{-1} V_1 m_u \right]$$
 (20)

 $\triangleright$  The value of  $V_2$  is given by:

$$V_2 = \frac{V_1}{\sin i_c} \tag{21}$$

The angle of slope of the dipping layer is found from:

$$\alpha = \frac{1}{2} \left[ \sin^{-1} V_1 m_d - \sin^{-1} V_1 m_u \right]$$
 (22)

The depths to the lower layer at either end of the shot line are found from:

$$Z_u = \frac{V_1 T_{iu}}{(\cos \alpha)(2\cos i_c)}$$
 (23)

$$Z_d = \frac{V_1 T_{id}}{(\cos \alpha) (2\cos i_c)}$$
 (24)

#### **5.1** Introduction

The term "water quality" is commonly used to describe the nonaqueous components of a volume of water. These can include suspended sediment, biota and dissolved species. In groundwater studies the latter i by far the most important, since the former two constituents are typically filtered out of recharging water during infiltration through a porous media. If an aquifer is strongly fractured or karstified, however, then suspended sediment and biota may persist during subsurface transport.

#### **5.2** The analysis of Groundwater Chemistry

The successful analysis of groundwater chemistry takes place in two stages, namely field practices and laboratory practices.

#### **5.2.1 Field Practices**

These are concerned with correct procedures at wells and springs. Fieldwork, must include on-site determinations of a number of parameters with may only be measured with any confidence before or immediately after the water leaves the ground.

- SAMPLE COLLECTION: Always collect duplicates of every sample, to allow for quality assurance in laboratory determinations. In general, aeration of samples should be avoided as far as possible.
- When collecting a sample from a well, always "purge" the well first, by withdrawing about three times the casing volume. This ensures that the water which reaches your sample bottle is "virgin" aquifer water, rather than water which has been in contact with the gravel pack and/or casing over an extended period of time.

Separate sample are required for the determination of organic and inorganic species. "Organic" samples must amount to about 2 liters, and must be collected in a brown glass bottle. The brown tint prevents photolysis organic species, and the glass will not adsorb the organic species as a plastic bottle would. If your glass bottle has a plastic cap, then line the interior with tin foil. After collection, the sample must kept refrigerated until extraction for chromatography (within 24 hours) and analysis (within a week).

"Inorganic samples" comprise the two sub-samples, one for cationdetermination, the other for anions. These samples are typically collected in plastic wide-mouthed 500 ml beakers, since glass can supply excess sodium to the water by leaching. The cation sample is acidified upon collection with about 3 ml (three of four pipette drops) of concentrated nitric acid, which prevents precipitation of carbonate and other compounds. The anion sample is not acidified. Both samples should be stored at a temperature close to that which they displayed at the time of collection. Analysis should be made as soon as possible, but the U.S, EPA have found that no serious departures occur if anion analysis is performed within a month, and cation within six months.

**ON-SITE MEASURMENTS:** the following parameters must always be measured on-site at the time of collection of corresponding samples:

#### 1. Temperature

- 2. **pH:** Portable battery driven battery driven meters are widely available, as are downhole probes, though the former are the cheapest and most versatile.
- 3. **Electrical conductivity:** Portable battery driven meters or a downhole probe, subject to funding.
- 4. Alkalinity: Titration with a hand-held "Hach" type digital titrator.
- 5. Redox potential, Eh: Downhole probe is the only realistic method.
- 6. Dissolved oxygen: Downhole probe or by titration.

Of the above six parameters, the first four are invariably measured, with the redox parameters (5 and 6) only being measured if there are plans to do geochemical analyses requiring their knowledge.

#### **5.2.2 Laboratory Practices**

**INORGANICS**: Many techniques are involved in the full determination of inorganic hydrochemistry with separate schemes for cation and anions.

Cations: Atomic Absorption Spectrophotometry (AAS) is the most popular and the best documented method. Samples are often extracted into nitric acid, by a lengthy mixing and evaporating process, to avoid matrix interferences.

#### The essentials of AAS are as follows:

Ground state atoms of an element are introduced into a "cell" (often a flame) in the path of a beam of resonance radiation (of wavelength corresponding to that of the element under investigation). The ground state atoms absorb this resonance radiation so that the radiation beam leaving the cell is somewhat reduced in intensity compared to the incident beam. The amount of absorbance measured can be related to the concentration of analyte elements in the flame.

All the major cations (Na, K, Ca, Mg) and many others are determined by AAS.

**2. Anions**: Numerous method s are in use in the determination of inorganic anions. They include titrimetry, spectrophotometry and colorimetry. Here, for example are the determination techniques for the major anions.

**Chloride**: An acidified sample is titrated against mercuric nitrate in the presence of a diphenylcarbazone/bromopho blue indicator. The endpoint is signaled by the precipitation of a blue-violet mercury complex suspension.

**Sulphate**: Barium is added to a quotient of the sample, and this causes precipitation of a lowly soluble barium sulphate. The turbidity of the resulting suspension is measured with a spectrophotometer operation at around 420 nm.

**Bicarbonate**: This is obtained by multiplication from the field titration value for alkalinity.

#### **5.3** How to Read Analysis

# 5.3.1 Objectives of the interpretation of hydrochemical data in GW investigations

- 1. To assess the suitability for the intended purpose.
- 2. To evaluate the corrosion and/or the incrustation potential of the GW with regard to the materials used as well as components.
- 3. To evaluate the likely origin of the GW.

#### 5.3.2 Units

The three units in common use for the expression of concentrations of dissolved species in groundwater are:

- ✓ Milligrams per liter mg/1 mass/volume
- ✓ Parts per million ppm mass/mass
- ✓ Milliequivalents per liter meq/1 mass, atomic mass, and charge volume

#### Some handy relations between units are:

- Mg/1 = ppm x relative density of the water (important when working with brines)
- ✓ Micrograms per liter, u/l = [mg/1]100
- ✓ Millimoles/I = [mg.1]/RAM, where RAN relative atomic mass.

#### **5.3.3** Milliequivalents

For geochemical porposes, it is often important to assess the mineral content of a water in a way that takes into account the differing charges and masses of the various dissolved ions. This is the purpose for which milloequivalents per liter are used, the definition is as follows:

Meq/1 = [mg/1][RAM/charge]

The ratio **[RAM/charge]** is known as the "combining weight" for a particular ion. In an analysis expressed in milliequivalents per liter, unit concentrations of all charged species are chemically equivalent, (uncharged species, such as SiO<sub>2</sub> can be taken into account by expressing them in millimoles/liter).

A corollary of this is that the sum if the concentration of all cations should equal that of the anions(in meq/1). if they do not match, then either (i) an important species has been neglected by the analyst, or (ii) the analysis is faulty.

The percentage diffrence between the cations and anions is known as the "cation-anion balance" (CAB) and should be calculated as a first step in interpreting a water analysis.

If CAB > 10% proceed with caution and look to see if any important analysis are missing from the report sheet. If CAB > 15% it is probably to discard the analysis.

$$CAB = \frac{[sum. of cations - sum. of anions]}{[sum. of cations + sum. of anions]} \times 100\%$$

#### **Examples:**

#### Convert the following from mg/l to meq/l

	Mg/I	atomic weight
Mg <sup>+2</sup>	63	24.32
NO <sub>3</sub> -1	5	N: 14, O: 16
SO <sub>4</sub> <sup>-2</sup>	15	S: 32.06
HCO-3	196	H: 1.008, C:12.1, O=16

Atomic weight; Mg= 24.32

Valence= 2

Equivalent weight= 24.32/2 = 12.16

63 mg/l Mg = 63/12.16 = 5.19 meq/l.

Molecular weight of  $NO_{3} = 1*14 + 3*16 = 62$ 

Valence= 1

 $5 \text{ mg/l NO}_{3} = 5/(62/1) = 0.08 \text{ meq/l}$ 

15 mg/l  $SO_4^{-2} = 15 / [(32.06 + 4*16) / 2] = 0.312 meq/l$ 196 mg/l  $HCO_3^{-2} = 196 / [(1.008+12.01+3*16) / 1] = 196 / 61.02 = 3.212 meq/l$ 

#### **5.3.3 The Common Components of Groundwater Analysis**

The following items are those you are most likely to encounter when reading a water analysis

**ALKALINITY**: This is the capacity of a solution to neutralise acid to a specified endpoint (usually pH 4.5 with a methyl orange indicator, or pH 8.3 with a phenolphthalein indicator). Several species ions dominate. For his reason alkalinity is usually expressed in terms of carbonate or bicarbonate concentrations, typically as "mg/1 as  $CaCO_{3-}$ " in most cases, the pH of natural waters is such that bicarbonate is the most abundant anion in the  $CO_2 - H_2O$  system. If pH is about 7, then the concentration of  $HCO_3$  in the water (in mg/1) may be calculated from an alkalinity value using the relation:

 $[HCO_3]$  = alkalinity (methy1 orange)/0.8202

**HARDNESS**: It is mainly caused by the presence if Ca and Mg in solution, which can react with soap to form a lowly soluble scum, and with bicarbonate ions to precipitate scale in kettles and boilers. The normal expression of hardness is "mg/l as CaCO<sub>3</sub>". This is related to the concentrations of Ca and Mg in solution by the following equation:

Hardness (mg/1 as  $CaCo_3$ ) = 2.5 [Ca] + 4.1[Mg]

Where the concentrations (approximately equal to activities, shown in [] type brackets) of Ca and contribute to this property.

#### **5.3.4 Notes on Important Inorganic Components**

**Iron (Fe):** Main natural sources: Dissolution of mafic minerals in igneous and metamorphic terrains; dissolution of iron rich cements in sandstones. Not usually abundant in waters from carbonate terrains.

**Soduim (Na):** Main natural sources: Plagiocalse feldspare in igneous and clastic sedimentary terrains; halite and nahcolite in evaporation terrains. Small amounts occur naturally in rainfall.

**Sulphate (SO<sub>4</sub><sup>-2</sup>):** Main natural sources: Oxidation of pyrite (which is an iron sulphate mineral) in igneous and sedimentary terrains (particularly in coal measures, leading to acidic mine drainage, and acid rain from coalfired power stations); dissolution of gypsum (CaSO<sub>4</sub>, 2H<sub>2</sub>O) and anhydrite, (CaSO<sub>4</sub>) in sedimentary terrains. Some organics will release sulphate on breaking down, thus making sewerage contamination a possible explanation for high sulphat if no natural source in obvious.

**Chloride (CL-1):** Main natural sources: Halite dissolution. Small amounts occur naturally in rainfall. Pollutant Cl<sup>-</sup> is very common, and occurs in human, animal. And industrial wastes, as well as from road de-icing salts. Chloride is very conservative chemically, and is therefore a good groundwater tracer, unlike sulphate, for instance, which is retarded by reactions.

**Fluoride (F<sup>-</sup>):** main natural sources: Apatite, mica, amphiboles, fluoride, (CaF<sub>2</sub> – lowly soluble) and from trace quantities in other widely disseminated minerals. Locally, volcanic or fumarolic gases may be an important source. Excessive F<sup>-</sup> causes mottling of tooth enamel. Teeth may become brittle because fluoride affects tooth density. Many Gaza children have this defect.

**Nitrate (NO<sub>3</sub><sup>-</sup>):** Usually reported as "nitrate as nitrogen (NO<sub>3</sub><sup>-</sup> - N)". To convert a  $NO_3$ <sup>-</sup> - N concentration to nitrate concentration, multiply the former by 4.4266. Main natural sources: Decaying legumes and other organic matter. Main sources today are always sewerage and nitrate fertilizers. A high concentration of Cl- together with NO3- is a more sign of sewerage pollution.

#### **5.4** Data Presentation and Interpretation

#### 5.4.1 Data Presentation

All of the common data plotting techniques in use in groundwater geochemistry require the data to be expressed in meq/l. Once a table of the data in meq/l has been prepared, the next step is to choose a plotting method which will suit the proposed use of the presentation. For the purpose of comparison and classification the ternary Durov and Piper plots are best, while Stiff diagrams, Pie diagrams and Maucha vector plots are ideal for use as mapping symbols.

**Piper Diagrams** are constructed as shown in **Figure 5.1**. The percentage meq/l totals of major anions and cations are first plotted in the small triangles, and then their interception in the diamond is determined and plotted. **Figure 5.2** shows the various HYDROCHEMICAL FACIES which are defined according to plotting positions on Piper Diagrams (see **Figure 5.3 and 5.4**).



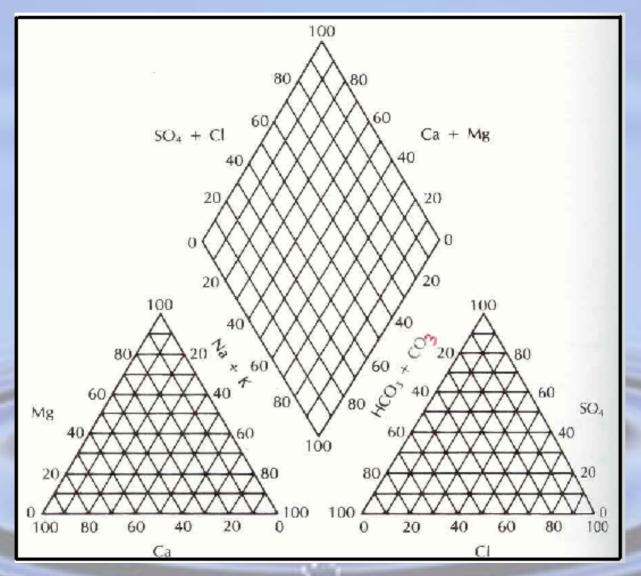


Figure 5.1: Piper diagram

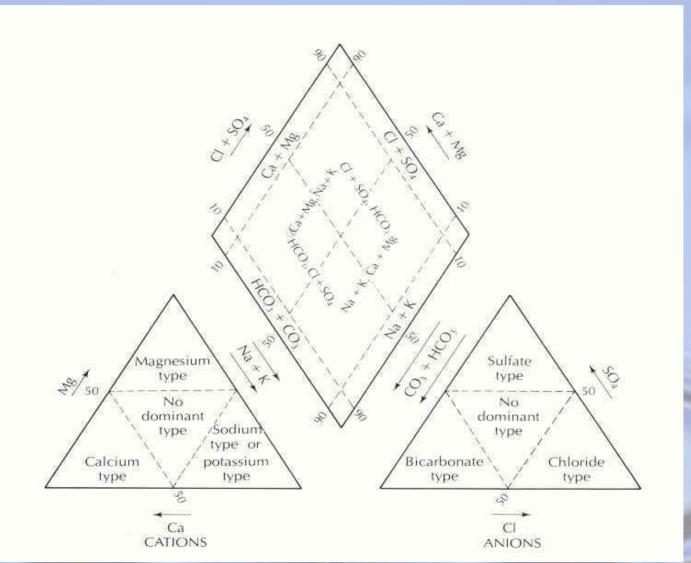


Figure 5.2: Hydrgeological classification system for natural waters using the Piper diagram

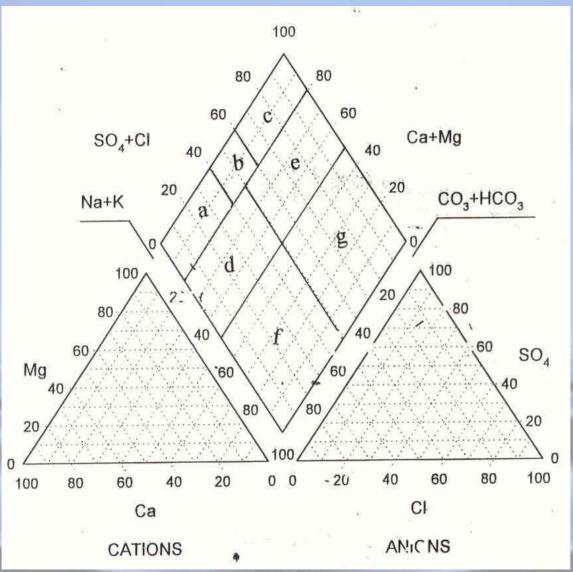
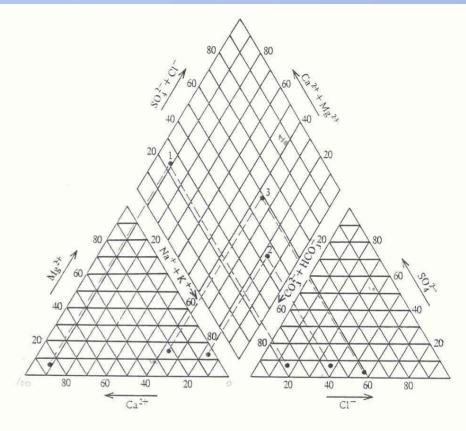


Figure 5.3: Piper diagram

- Normal earth alkaline water
  - a. with prevailing bicarbonate
  - b. with bicarbonate and sulphate (or chlorine)
  - c. with prevailing sulphate (or chloride)
- Earth alkaline water with increased portion of alkalies
  - a. with prevailing bicarbonate
  - b. with bicarbonate and sulphate
- Alkaline water
  - a. with prevailing bicarbonate
  - b. with bicarbonate and sulphate-chloride

Figure 5.4 Example of using
Piper diagram. The same example
will be solved by using Durov
Diagram in the next bage



	mg I - i meg l - i Per cen		
	mg t	med I	Percent
Ca <sup>2+</sup>	152	7.58	85.5
$Ag^{2+}$	5.3	0.48	5.4
la <sup>+</sup>	17	0.74	8.3
-	2.8	0.07	0.3
ICO <sub>3</sub>	404	6.61	77.7
01-	29	0.60	7.1
11-	46	1.30	15.2

mg l <sup>-i</sup>	meq 1 <sup>-1</sup>	Per cent
8	0.40	4.0
15.5	1.28	12.3
136	8.09	81.4
7	0.18	1.3
326	5.34	55.8
37	0.77	8.0
123	3.47	36.2

mg l <sup>-i</sup>	meq l-t	Per cent
85	4.24	22.3
35	2.38	15.2
270	11.74	61.3
6	0.15	2.3
479	7.84	40.6
29	0.60	3.1
286	10.39	56.3

**Durov Diagrams** closely resemble Piper Diagrams, but allow additional plotting of pH and TDS (see **Figure 5.5** and **Figure 5.6**).

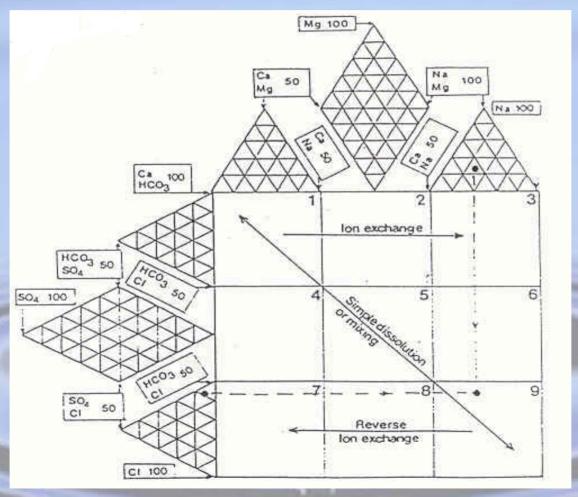


Figure 5.5: Expanded Durov Plot

**Expanded Durov Plot**: Significance of the nine fields shown in **Figure 6.5** are:

- **1. HCO**<sub>3</sub><sup>-</sup> **and Ca**<sup>2+</sup> dominate. Frequently recharging waters in limestone, sandstone and many types of aquifers.
- **2.** HCO<sub>3</sub><sup>-</sup> and Mg<sup>2+</sup> dominate, or cations dominance indiscriminate with Ca<sup>2+</sup> and Mg<sup>2+</sup> important. Often indicates waters associated with dolomites; where Ca<sup>2+</sup> and Na<sup>+</sup> are important then partial ion exchange may be indicated.
- **3.** HCO<sub>3</sub><sup>-</sup> and Na<sup>+</sup> dominant. Normally indicates ion-exchanged waters, although the generation of CO<sub>2</sub> at depth can produce HCO<sub>3</sub><sup>-</sup> where Na<sup>+</sup> is dominant under certain circumstances.

- **4.** SO<sub>4</sub><sup>2-</sup> dominant or anions dominance indiscriminate, and Ca<sup>2+</sup> dominant. Ca<sup>2+</sup> and SO<sub>4</sub><sup>2-</sup> dominant often indicates recharge through gypsiferous deposits or lavas; otherwise a mixed water or simple dissolution (e.g. gypsum, anhydrite, epsomite) may be indicated.
- **5. No dominant anion or cation species.** Indicates waters exhibiting simple dissolution or mixing.
- **6.** SO<sub>4</sub><sup>2-</sup> dominant or anions dominance indiscriminate, and Na<sup>+</sup> dominant. An unusual water type, probably reflects mixing.
- 7. Cl<sup>-</sup> and Ca<sup>2+</sup> dominant. Again an unusual water type unless cement pollution is present in a well; otherwise may arise from reverse ion-exchange of Na<sup>+</sup>-Cl<sup>-</sup> waters.

- **8.** Cl<sup>-</sup> dominant, and cations indiscriminate. Indicates that waters are related to reverse ion-exchange of Na<sup>+</sup>- Cl<sup>-</sup> waters.
- **9. CI**<sup>-</sup> **and Na**<sup>+</sup> **dominant,** frequently represents mixing end-menber waters. Durov plot does not allow distinction between Na<sup>+</sup>-Cl<sup>-</sup> water, or evolution e.g. by seawater mixing or halite dissolution.

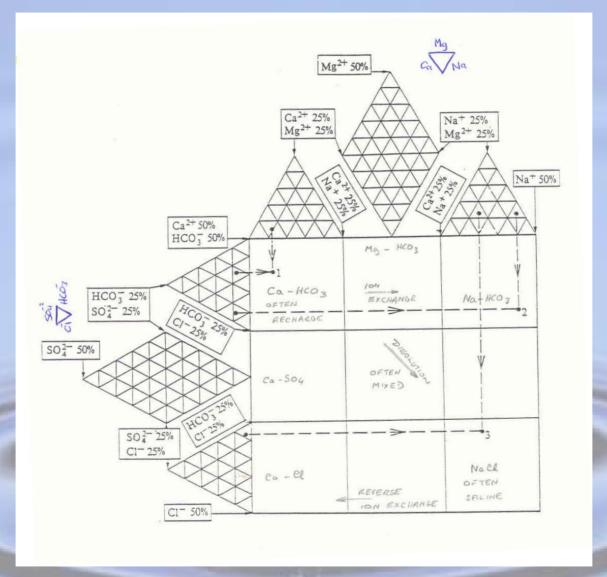
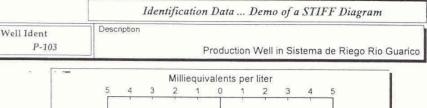
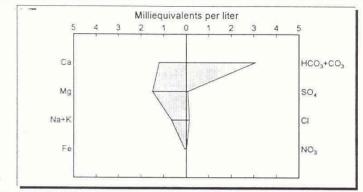


Figure 5.6: Expanded Durov Diagram. (points 1,2, and 3) are the same in Figure 5.4

**Stiff Diagrams** (see **Figure 5.7**) are polygons representing the major ion distributions of water samples. They make excellent mapping symbols,

Figure 5.7: entry and reporting form of Stiff diagram





Cations					
	Ca	Mg	Na	K	Fe
Milliequivalents per liter	1.2001	1.4897	0.5999	0.03989	0.0645
Milligrams per liter	24.05	18.11	13.79	1.56	1.20

		Anions			
	HCO3	CO3	SO4	Cl	NO3
Milliequivalents per liter	3.08001	0.0000	0.07995	0.15008	0.03387
Milligrams per liter	187.92	0.00	3.84	5.32	2.10

Mn	NO2	PO4	F	В	SIO2
TDS 255.00	Hardness	Alkalinity	Conductivity 300.00	pH 6.80	SAR 0.5173

Water Type	Magnesium Bicarbonate	Cations (epm) 3.39	Anions (epm) 3.34
**************************************	3,000	Terrier.	1

Error Balance 1.49

**Pie Diagrams** (see **Figure 5.8**) are constructed so that the radius indicates the TDS content of the water.

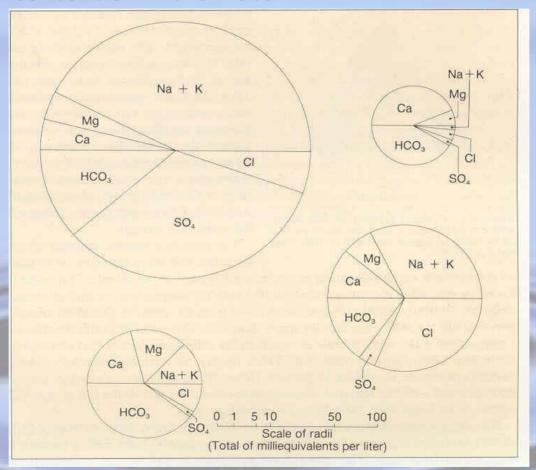


Figure 5.8: Four analysis represented by circular diagrams (Pie Diagrams) subdivided on the basis of percentage of total milliequivalents per liter.

#### **5.4.2 Hydrochemical Facies**

The facies are function of the lithology, solution kinetics, and flow patterns of the aquifer.

#### **5.4.3** Isotope Hydrogeology

**Isotopes** for a particular element have the same atomic number but different atomic weights due to varying numbers of neutrons in the nucleus. **Stable and Radioactive isotopes**.

#### > Stable Isotopes

H, O, C, N, S stable isotopes can be used to study geological processes that affect ground and surface waters.

- Radioactive Isotopes
- ✓ To determine the direction and/or velocity of GW flows.
- ✓ Age dating:
  - <sup>3</sup>H- (Trictium), half-life = 12.3y. In the atmosphere it is in the form H<sup>3</sup>HO and enters the GW as recharging precipitation. <sup>3</sup>H has been used to trace the seepage of contaminated GW from low level nuclear waste disposal areas. <sup>14</sup>C, half-life, = 5730y.

#### **5.4.4 Interpretation of Groundwater Chemistry**

Methods use to sample GW for **Carbon Isotope analyses**: 14X and S13C isotope analyses are generally taken from GW by precipitation. This method uses the principle of rendering the solution sufficiently alkaline (pH>8). So that aqueous  $\mathbf{CO_3^{-2}}$  is continually available for reaction to precipitate an insoluble carbonate compound.

Processes affecting the Carbon Composition of GW without affection the Carbon Concentration:

#### a) Isotope exchange

This involves the exchange of carbon atoms between groundwater and other carbon sources such as aquifer carbonates.

# b) Incongruent dissolution of carbonate or dissolution precipitation

Together with the soil  $CO_2$  -carbonate reaction, incongruent dissolution reaction are considered of dominant importance in controlling the carbon isotope compositions of most carbonate groundwaters.

Incongruent dissolution typically involves the solution of relatively impute carbonates with the consequent precipitation of more pure carbonates. For example, in the Triassic sandstones dolomite  $(CaMg(CO_3)_2)$  is dissolved and calcite  $(CaCO_3)$  precipitated. In purer  $CaCO^3$  rocks such as the Chalk and Lincolnshire Limestone other incongruent dissolution reactions occur.

#### 14C AGE CORRECTION METHODS

There are numerous methods for producing of corrected 14C ages for groundwaters, with perhaps the most renowned and comprehensive works being those of Wigley et.al. (1978), Fonts and Grainer (1979) and Reardon and Fritz (1978) the simple age correction method considered below is that of Wigle (1976) and considers a groundwater where the initial carbon is generated from a reaction between soil  $CO_{-2}$  and rock  $CaCO_{3}$ , and then is affected only by incongruent dissolution of rock carbonate in the aquifer and  $^{14}C$  decay.

The simple **carbonate equation** for the unsaturated zone is :

$$H_2O$$
 (recharging water) +  $CO_2(Soil)$  +  $CaCO_3$  (rock) =  $Ca(HCO_3)_2$  (bicarbonate)

To consider a simple 50% dilution the  $\delta^{13}$  of the bicarbonate is -13% and the <sup>14</sup>C content is 50pmc ( $\delta^{13}$  CO<sub>2</sub>=26%, <sup>14</sup>C=100pmc;  $\delta^{13}$ C CaCO<sub>3</sub> =0%, <sup>14</sup>C = 0 pmc). This is a simplified starting isotopic composition of a recharging groundwater and is an inert media, in which no further carbonate dissolution or precipitation could occur, groundwaters could simply be dated using the decay law:

$$t = 8267 \log_{e} \left(\frac{A_{0}}{A_{t}}\right) \longrightarrow t = 8267 \log_{e} \left(\frac{A_{0}X}{A_{t}}\right)$$

$$X = \frac{2.5 + S^{13}C - S^{13}Cr}{S^{13}C_{0} - S^{13}Cr + 2.5}$$

Where,

T = time in years or apparent age of the water

8267 = the mean life of  ${}^{14}C = [T_{1/2} log_e^2]$ 

 $A_t$  = the <sup>14</sup>C content of the sample

 $A_0$  = the <sup>14</sup>C content of a zero age aground water (in this example 50 pmc)

However, as stated before incongruent dissolution of rock carbonate occurs in many aquifers and to facilitate correction for this phenomenton, account is taken of the stable isotope  $\delta^{13}$  C ratios of the groundwater and the rock matrix. Correction, methods have also to consider preferred fractionation of <sup>14</sup>C over <sup>13</sup>C. Fractionation is a tem applied to the relative partitioning of isotopes in reactions, etc. Due to differences in the physical and chemical properties of the isotopes. In reactions governing <sup>14</sup>C, <sup>13</sup>C and <sup>12</sup>C, E<sup>14</sup>C is generally assumed to equal 2E<sup>13</sup>C (E is called an enrichment factor and is more convenient way of expressing a fractionation factor).

To correct for incongruent dissolution of carbonate down a groundwater flow path wigley, (1976) has devised the following correction factor:

$$X = \frac{2.5 + \delta^{13}C - \delta^{13}Cr}{\delta^{13}C_0 - \delta^{13}Cr + 2.5}$$

Where,

**2.5** = E between rock and solution in ‰, although this does vary with pH and temperature

 $\delta^{13}$ C is ratio for water

 $\delta^{13}Cr$  is ratio for rock(‰ in this example)

 $\delta^{13}C_0$  is original ratio of groundwater recharge, -13‰ in this example.

The 14C dated of groundwaters are evaluated using the equation:

$$t = 8267 \log_e \left(\frac{50X}{A_t}\right) years$$

#### **Example:**

For Groundwater same collected with  $^{14}C=30$  Pmc,  $\delta^{13}C=-12\%$ 

$$X = \frac{2.5 - 12 - 0}{-12 - 0 + 2.5} \longrightarrow X = 0.905$$

$$t = 8267 \log_e \left(\frac{50 \times 0.905}{30}\right) years \longrightarrow t = 3398 years$$

#### **5.4.5 Water Rock Interactions**

Groundwater tends to show an increase in TDS with age, andtherefore with depth. Though other factors may operate, the chief reason for this phenomenon is that the longer the water is in contact with rock the more change there is for the minerals to dissolve. A corollary of this is that fast-moving groundwaters will be less mineralised than slow-moving groundwaters following a flowpath of the same length.

Dissolution of minerals by groundwater is an example of CHEMICAL

#### WEATHERING and it depends on:

- 1. The composition of the rocks.
- 2. The solubility of the rock-forming minerals.
- 3. The saturation characteristics of the water with respect to these minerals.

#### How to evaluate incrustation and corrosion of GW Potential

1) Eh is a measure of the relative activities of the oxidsed and reduced ion existing in a system. Eh can help in determining the stability of iron (Fe) Species and hence corrosion.

#### The redox reaction for iron (half reaction):

$$O_{2+}4H^{+} + 4e = 2H_{2}O \text{ reduction}$$
 $4Fe^{2+} = 4Fe^{3+} + 4e \text{ (oxidization)}$ 

pE = -log[e]

PE: dimension less quantity used to describe the relative electron activity.

$$pE = 12.53 + log[Fe^{3+}/Fe^{2+}]$$

pE=16.9 Eh

Eh: Redox potential (volts)

2) Incrustation potential is best determined using the saturation indices of common calcium salts such as calcite, dolomite and gypsum.

$$SI = \log \frac{IAP}{Ksp}$$

SI: saturation index

IAP: ion activity product

Ksp: solubility constant of mineral phase

SI= 0, gw is in equilibrium with the mineral phase

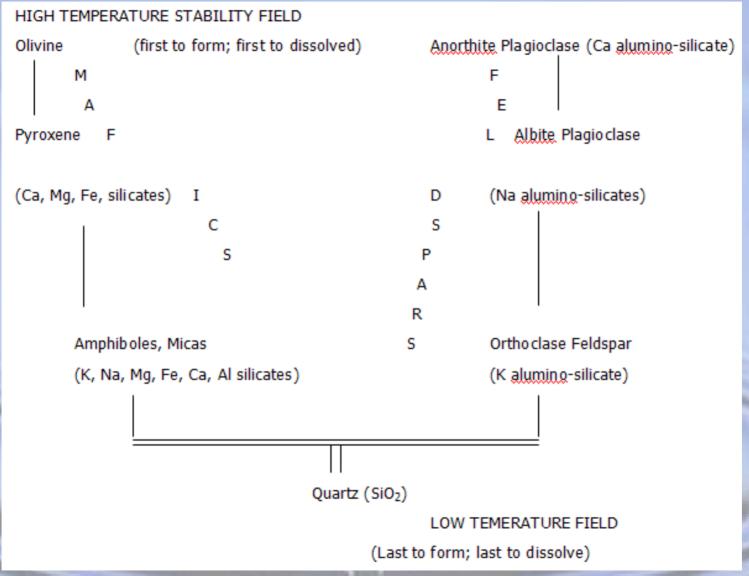
SI>0, gw is supersaturated with the mineral phase

SI<0, gw is subsaturated with the mineral phase

>THERMODYNAMICS is the branch of chemistry which deals with the kinetics of dissolution and precipitation. Saturation indices and solubility products are calculated for the water and the rock in system under investigation, allowing predictions of the behavior of the water to be made. Computer programmes are in common use for performing such work including the well-known WATEQ and WATEQF programmes of the U.S. Geological Survey. Such programmes have been used recently to investigate the evolution of groundwater chemistry as the water flows through a varied sequence of rocks.

- Such model simulation have illustrated the importance of the "order if encounter" of a groundwater with various rocks in determining the "final" groundwater chemistry as realized in a spring or borehole sample.
- The partial pressure of CO<sub>2</sub> in the soil zone exerts a profound influence on the hydrogeochemistry of carbonate aquifers. This is because the ease with which water will dissolve minerals in the Ca-H<sub>2</sub>O-CO<sub>2</sub> system is dependent on the dissolved CO<sub>2</sub> content of the water. It is for this reason that the karstification of aquifers only occurs in carbonate aquifers where they are overlain by an appreciable blanket of soil or fine grained clastic sediments. Hence "order of encounter" is critically important in carbonate aquifer systems.

The susceptibility of minerals to dissolution depends on their stability at temperatures and pressure obtaining during contact with thermodynamically under saturated groundwater. Many minerals found in igneous and metamorphic rocks were formed at elevated temperatures and pressures and are unstable in the normal range of temperatures and pressures encountered in shallow groundwater system. Only low matrix hydraulic conductivities prevent wholesale dissolution of rocks containing such minerals (i.e. igneous and metamorphic rocks and the clastic sedimentary rocks derived from them). The order in which the igneous minerals will be dissolved is given by Bower's Reaction Series which is a scheme of the order in rock material (magma). A simplified version of the scheme is giver below.



FURTHER CONTROLS ON GROUNDWATER COMPOSITION includes cation exchange diffusion into storage and membrane filtration. Cation exchange is the group of processes whereby cations (most notably Ca and Na) are adsorbed and desorbed by clay minerals (especially montmorillonite). When Ca is taken up by sodic montmorillontitem, Na will be released.

Ca(5 meq/1) + Na (3 meq/1 ) Na - Mont. Ca(3)+Na(5) +CL(3meq/1) +SO<sub>4</sub>(5 meq/1) 
$$\rightarrow$$
 Na + Cl(3) + SO<sub>4</sub>(5)

Note in the above example how the equal concentrations in meq/1 of Na and C1 (from halite dissolution) and Ca and  $SO_4$  (from gypsum) are altered when cation exchange removes Ca from the water and supplies Na.

- DIFFUSION INTO MATRIX STORAGE is a process thought to occur in some "dual porosity "system, i.e. fractured media which also have matrix porosity. The anomalously low tritium and nitrate concentrations in water from the Chalk aquifer of solution. England have been explained by invoking this process, whereby the solute molecules pass into storage in the inter-fracture blocks even though advection occurs primarily in the fractures.
- When water is forced across a semi-permeable membrane by high hydraulic heads the water will cross but not all of the solutes. Solute ions and molecules with large radii will remain behind, so that the remnant water increase in TDS content. In deep sedimentary basins, mudstone horizons appear to act as semi-permeable membranes and thus the "membrane effect" is a process which increases still further the high TDS of deep groundwaters noted above.

How to assess GW suitability for drinking water and irrigation puposes:

#### 1) Drinking purposes

i) Drinking water standards (see **Table 5.1**)

ii) Hardness

Hardness (mg/l)	class
0-75	soft
75-150	moderately hard
150-300	hard
>300	Very hard

#### 2) Irrigation

$$SAR = \frac{Na^{+}}{\sqrt{\frac{Ca^{++} + Mg^{++}}{2}}} \qquad \% Na = \frac{Na^{+} + K^{+}}{Ca^{++} + Mg^{++} + Na^{+} + Ka^{+}} \times 100$$

%Na	EC(uS/cm)	Class
<20	<250	Excellent
20-40	250-750	Good
40-60	750-2000	Permissible
60-80	2000-3000	Doubtful
>80	>3000	Unsuitable

A simplified seven-step mass balance routine for the preliminary interpretation of water analyses is presented below. It was devised by Dr. A.W. Hounslow of Oklahoma State University (Personal Communication, 1985) and is based on the calculations and discussion pf Garrels and Mackenzie (1967; see recommended reading list). While not infallible and not meant to replace the more refined thermodynamic models such as WATEQ, this method can at most be very helpful, or at least help to remove some of the confusion from water analysis interpretation.

- STEP 1: Check pH. If less than 6, abandon the project.
- **STEP 2**: Change all consecrations into meq/1 (millimoles/1 for uncharges SiO<sub>2</sub>).
- **STEP 3**: Calculate the CAB. If CAB > 5% Proceed with caution or throw the analysis out.
- **STEP 4**: Compare the C1 and Na contents. Primary assumption is that C1 is from sodium chloride, either directly or from the ocean via precipitation. Na can come from other sources, e.g. feldspar dissolution or caution exchange. Thus if C1>Na, then either the analysis is faulty or the water derived its composition from the dissolution of evaporate minerals (e.g. halite). In the latter case, on would expect the TDS to be high at least over 500mg/1. If Na is greater than or equal to C1, go to 5.

**STEP 5**: Compare the Ca and  $SO_4$  contents. Primary assumption is that  $SO_4$  is the result of direct dissolution of gypsum or the neutralization of acid waters by limestone or dolomite. In the latter case, Mg may be prominent. If  $SO_4 > Ca$ , then the inference is that Ca has been removed from solution most likely by precipitation of calcite or caution exchange. If  $Ca > So_4$ , go to 6.

**STEP 6:** Compare  $HCO_3$  with  $SiO_2$ . Bicarbonate is formed when  $CO_2$  and  $H_2O$  react with various minerals in a process called acid hydrolysis. Carbonates dissolve without releasing  $SiO_2$  whereas albite dissolution releases considerable  $SiO_2$ , with smaller quantities from the dissolution of other silicates. An arbitrary division of  $SiO_2/HCO_3 = 0.1$  is used to indicate silicate versus carbonate weathering (i.e. if  $HCO_3 > 10*SiO_2$ , carbonate weathering is indicated; otherwise continue to Step

**STEP 7:** Compare  $SiO_2$  with [Na+K-C1]. It is assumed that after subtracting the C1 from Na, the remaining Na is due to the weathering of plagioclase and the K from the weathering of biotite and (to a lesser extent) potash feldspar (orthoclase). If other mafic minerals contributed then  $SiO_2$  will be present in a considerable excess over Na+K. It is further assumed that the solid weathering product is kaolinite or montmorillonite; the former releasing more  $SiO_2$  to the water than the latter. Hence we may conclude that if:

- **a.**  $SiO_2 > 2*[Na+k-C1]$ , then the minerals subjected to weathering included a considerable quantity of mafics (olivine, pyroxene, amphibole, etc.) This being the case, most of the Ca will be from weathering of anorthitic plagioclase.
- **b.**  $SiO_2 < [Na+k-C1]$  then cation exchange is probably the source of most of the excess Na, in which case it is probable that  $Ca < SO_4$ .
- **c.** [Na+K-C1] <2\*[Na+k-C1] then Na feldspar weathering is suspected with solid product of kaolinite or montmorillonite.

The <sup>14</sup>C Dates of groundwaters are evaluated using the equation:

$$t = 8267 \log_e \left(\frac{50X}{A_t}\right) years$$

Example:

Groundwater sample collected with  $^{14}\text{C}=30$  Pmc,  $\delta^{13}\text{C}=-12\%$ 

$$X = \frac{2.5 - 12 - 0}{-12 - 0 + 2.5} \longrightarrow X = 0.905$$

$$t = 8267 \log_e \left(\frac{50 \times 0.905}{30}\right) years \longrightarrow t = 3398 years$$

Increase    Table 5.1:   Drinking water standards		Constituent	(mg/ <i>l</i> )
Arsenic (As) Barium (Ba)  Arsenic (As) Barium (Ba)  O.05 Barium (CrVI)  Cadminum (CrVI)  O.01 Chromium (CrVI)  Selenium  Antimony (Sb)  Lead (Pb)  Mercury (Ig) Silver (As) Fluoride (P)  Cyanide  Cyanide  Cyanide  Cyanide  Cyanide  Cyanide  Cyanide  Cyanide  O.05 Endrine  O.0002 Lindane  Methoxychlor  O.1 Toxaphene  O.005  2,4-D  O.1  2,4,5-TP silvex  O.01  Phenols  O.01  Phenols  Radionuclides and radiosctivity Radium 226  Stotontium 90  Plutonium  So,000  Gross beta activity  Radium 226  Stotontium 90  Plutonium  So,000  Gross beta activity  Radium 226  Stotontium 90  I D  Plutonium  So,000  Gross beta activity  3  Bacteriological  Total coliform bacteria  I per 100 mt  sourcess: U.S. Environmental Protection Agency, 1975 and World  Halth Organization, European Standards, 1970.  *Recommended concentration limits for these constituents are mainly	Table 5.1: Drinking water standards	Total dissolved solids Chloride (Cl) Sulfate (SO <sub>4</sub> <sup>2-</sup> ) Nitrate (NO <sub>3</sub> ) Iron (Fe) Manganese (Mn) Copper (Cu) Zinc (Zr) Loron (B)	250 250 45† 0.3 0.05 1.0 5.0
Arsenic (As) 0.05 Barium (Ra) 1.0 Cadmium (CA) 0.01 Chromium (CYI) 0.05 Selenium 0.01 Antimony (Sb) 0.01 Lead (Pb) 0.05 Mercury (Hg) 0.002 Silver (Ag) 0.03 Fluoride (F) 0.05 Fluoride (F) 0.05 Fluoride (F) 0.05 Fluoride (F) 0.05 Endrine 0.0002 Lindane 0.004 Methoxychlor 0.1 Toxaphene 0.004 Methoxychlor 0.1 Toxaphene 0.005 2,4-D 0.1 2,4,5-TP silvex 0.01 Phenols 0.001 Carbon chlorofgrm extract 0.2 Synthetic detergents 0.5 Radionactivity (pCi(I) Radium 226 Strontium 90 10 Plutonium 50,000 Gross beta activity 30 Gross alpha activity 30 Gross alpha activity 3 Bacteriological Total coliform bacteria 1 per 100 mt  sourcess: U.S. Environmental Protection Agency, 1975 and World Halth Organization, European Standards, 1970. **Recommended concentration limits for these constituents are mainly			
Barium (Ba)			
Cadmium (Cd)			
Selenium			
Antimony (Sb) 0.01  Lead (Pb) 0.05  Mercury (Hg) 0.002  Silver (Ag) 0.005  Fluoride (F) 1.4-2.48  Organic  Cyanide 0.05  Endrine 0.0002  Lindane 0.004  Methoxychlor 0.1  Toxaphene 0.005  2.4-D 0.1  2.4,5-TP silvex 0.01  Phenols 0.001  Carbon chloroform extract 0.2  Synthetic detergents 0.5  Radionuclides and Maximum permissible activity (radioactivity)  Radioactivity (pCU/t)  Radiom 226 5  Strontium 90 10  Plutonium 50,000  Gross beta activity 30  Gross alpha activity 3  Bacteriological Total coliform bacteria 1 per 100 mt  sources: U.S. Environmental Protection Agency, 1975 and World Health Organization, European Standards, 1970.			
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		Health Organization, European Stand	dards, 1970.
to provide acceptable esthetic and taste characteristics			

to provide acceptable esthetic and taste characteristics.

Recommended concentration limit\*

†Limit for NO3 expressed as N is 10 mg/t according to U.S. and Canadian standards; according to WHO European standards, it is 11.3 mg/l as N and 50 mg/l as NO3.

Flow chart using illustrating logic of water quality interpretation using

simplified mass

balance technique

